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THE EFFECT OF ALTERNATIVE BUFFERING TECHNIQUES TO PROTECT A
MULTI-PRODUCT, MULTI-STAGE PRODUCTION INVENTORY SYSTEM
AGAINST SUPPLY-UNCERTAINTY

The Louisiana State University and Agricultural and Mechanical Col.

PH.D. 1983

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THE EFFECT OF ALTERNATIVE BUFFERING TECHNIQUES
TO PROTECT A MULTI-PRODUCT,
MULTI-STAGE PRODUCTION INVENTORY SYSTEM
AGAINST SUPPLY UNCERTAINTY.

A Dissertation

Submitted to the Graduate Faculty of the
Louisiana State University and
Agricultural and Mechanical College
in partial fulfillment of the
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Doctor of Philosophy

in

Business Administration

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ABSTRACT

This research has been an experimental investigation of some of the operational aspects of a hypothetical multiproduct, multistage production inventory system operating in a supply uncertainty environment.

The main objective of this study was to explore the relative effect of different multilevel buffering strategies on system performance in order to establish some guidelines for choosing among different buffering techniques when buffering the system against different conditions of supply uncertainty. Several performance criteria, including holding cost, inventory cost, total cost, number of shortages, number of stockouts, service level and buffering cost effectiveness, were used to evaluate system performance.

The independent variables investigated include: buffering strategy (6 strategies), type of supply uncertainty (4 levels), and degree of supply uncertainty (4 levels). Five replications were generated for each of the 96 cells in the three-factor, full factorial experimental design. The main effect for each factor and the interaction effect for different combinations were considered.

Results show that performance of the production system is significantly influenced by the "buffering strategy" factor, although the relative impact of the six buffering strategies is dependent on the performance measure considered. The study also shows that both uncertainty type (quantity and timing) and uncertainty level (high and low) have significant impact on system performance. Moreover, interaction between buffering strategy and either uncertainty type or uncertainty level, were also found to be important in several cases. Overall, this research

provides empirical evidence that both supply uncertainty type and level are significant decision variables regarding the selection of an appropriate buffering strategy.

CHAPTER ONE

INTRODUCTION

When manufacturing a complicated product, it is often a problem to get the appropriate number of materials made (or purchased) and ready at the right time to assemble into the end or final product.

Materials Requirements Planning (MRP) has been introduced as a means of approaching this problem. Such a system (sometimes called "time phased requirements planning") embodies a logic designed expressly for companies with assembled products whose parts and raw materials have a demand that is, for the most part, dependent upon the demand for the finished goods. When demand for items is derived from plans to make certain products, as it is in the case of raw materials, parts, and sub-assemblies which are used in producing a finished product, those items are said to have dependent demand. Conversely, demand for a finished product is independent in the sense that it cannot be based on demand for some higher-level item. MRP is a set of procedures and decision rules designed to determine requirements of inventoried items, as to both quantity and timing, on all levels below the end product. Most of the developmental work on MRP was done by Joseph Orlicky, Oliver Wright, and George Plossl (34, 47, 59) and through the support of the American Production and Inventory Control Society (46). Today these methods are widely used in computer based production and inventory planning and control systems associated with hierarchial, multistage production process (18).

Description of the Problem

As an explosion-based system, MRP derives the demand for dependent items from a master production schedule that projects finished goods

production into the future. The exploding process is simply a multiplication of the number of end items by the quantity of each component required to produce a single end item. The explosion identifies what components are required, as well as how many, to produce a given number of end items as specified in the master production schedule. Because the master schedule reflects the planned production of finished goods, the MRP system, ideally, must determine only the true and exact requirements of inventory component items. Though it is possible to operate a requirements planning system on the basis of no buffering or safety stock, uncertainty from various sources typically requires the use of some buffering strategy to avoid disruption of the production process.

There are at least two types of uncertainty with which the MRP system must be able to cope: demand uncertainty and supply uncertainty. Demand uncertainty occurs when the master schedule is increased or decreased to reflect changes in the quantity and/or timing of customer orders or other factors affecting production requirements. This will cause changes in lower level items' requirements. The second source of uncertainty is supply uncertainty which originates from variations in the supply schedule. The time required for processing and filling component orders by an internal supplier is variable because of such factors as delays and breakdowns. In addition, the actual quantity delivered from production is variable because of scrap losses or shortages of lower level materials. Outside purchases are also subject to supply uncertainty. Orders from vendors are subject to uncertainty because of variability in both production and transportation times.

The problem of uncertainty is studied in detail in the classical inventory literature. A substantial body of knowledge exists on the

use of safety stock as a buffering strategy in statistical inventory management system (Economic Lot Size/Reorder Point Systems) (for example see: 8, 26, 33, 54). In a very comprehensive article, Tersine (36) outlined the procedures available for developing safety stock levels under conditions of known and unknown stockout cost for discrete and continuous distributions of usage during lead time. These procedures are designed mainly for independent demand items with the assumption that demand is constant. Most dependent demand items in a multiechelon inventory structure exhibit "lumpy" demand patterns. This lumpiness occurs because most manufacturing is in lots and all items needed to produce the lots are usually withdrawn from inventory at the same time, not unit by unit. A major assumption upon which conventional inventory control models are based (constant demand) is violated, thus such inventory systems are not readily applicable in these cases. If one attempts to adapt the use of this type of system by employing average demand rate, unexpected stockouts of components occur because of the lumped nature of the requirements, which upsets assembly schedules.

On the other hand, there has been little research on how to protect manufactured parts, subassemblies, or final assemblies against demand and supply uncertainties in a production system using MRP technique. In 1975, New (41) reported that there has been little reference to the problem of setting safety stock levels in MRP systems. After about eight years, it seems that this is still the case especially if the problem of different buffering strategies is considered.

Most of the research in this area has been limited to the use of safety stocks as the only technique available to protect the production process against uncertainty. This type of research might be considered

as an extension of the classical inventory analysis, using mostly mathematical and statistical techniques. Researchers have not considered some of the other buffering alternatives that might be used in an MRP system to protect against uncertainty. New (41) introduced three methods available to protect the system against both supply and demand uncertainty. These are fixed quantity buffer, safety lead time, and increased master schedule. Whybark and Williams (58) mentioned that to protect the part against uncertainty, several alternatives are available, varying from inventory oriented buffering techniques to frequent replanning with sufficient capacity and flexibility to accommodate the new plans. In their study, however, they restricted their attention to evaluating two inventory oriented buffering techniques: safety lead time and safety stock.

Another major shortcoming in this area of research is that only demand uncertainty has received much attention (for example see: 4, 11, 19, 35, 39, 42). The use of some demand forecasting techniques was always introduced as a way of reducing demand uncertainty (21, 42). The effect of end-item demand variability and uncertainty on the production system performance and lot size selection has also been mentioned in the literature (11, 12). On the other hand, supply uncertainty has not received an equal research effort and study in spite of the fact that supply uncertainty is anticipated to be a common factor in the future. Buffa (9) expresses it as follows:

".... materials will become more and more scarce. Good operations management may be the result of managing with scarce or uncertain supply

.... If the environment were to change so that uncertainty of supply were a common factor, then the focus of operations management would also need to change."

The need for a comprehensive study of this problem has frequently been mentioned. In a rather comprehensive survey of the problem, New (41) reported that little guidance has been offered to the manager in selecting a buffering procedure appropriate to his operating environment. In 1976, Whybark and Williams (59) stated that a systematic study to provide guidelines for the use of safety stock or safety lead time is required. Therefore, the theme of this research is to study the effect of different multilevel (joint) buffering techniques when used to protect a multi-state production-inventory system against quantity and timing supply uncertainty in an MRP system. A joint buffering strategy as used in this study is a combination of different buffering techniques (safety stock and safety lead time) applied to different levels of the product structure. A joint uncertainty, on the other hand, will indicate a combination of different types (quantity, timing) and levels (high, low) of supply uncertainty applied to different levels of product structure. This study will attempt to accomplish two objectives:

- (1) Provide some insights into the behavior of a production-inventory system facing different conditions of supply uncertainty when using different buffering strategies. Therefore, exploring the relative effect of different joint (multilevel) buffering strategies on the performance of a production-inventory system will be possible.
- (2) Establish some guidelines for choosing among different buffering techniques when buffering the system against different combinations of supply uncertainty types and levels.

Scope and Limitations of this Research

This study is intended to provide new information concerning the applicability of joint buffering strategies in a multistage production-inventory system using MRP. Moreover, this study will contribute to the current body of knowledge by assessing the effects of various factors on the performance of a multiechelon production-inventory system. These are: (1) multilevel (joint) buffering strategies, (2) degree of supply uncertainty, and (3) type of supply uncertainty. The main effect for each factor and the interaction effect for different combinations will be considered for various system performance measures.

To protect the system against uncertainty, several alternatives are available as mentioned above. In this research only two inventory oriented buffering techniques, safety stock and safety lead time, are considered. Uncertainty of supply will be the only source of risk considered. Limiting the scope of this study in this manner allows concentration on the influence of different types and levels of supply uncertainty on the buffering strategies.

In this study, the literature most relevant to this research is reviewed in Chapter II. Methodological and technical aspects of the study are pointed out and attempts are made to resolve these issues in Chapter III. The main purpose of the chapter is to describe the simulation system that is used and the procedures that incorporate risk into the system at each inventory level. The statements of hypotheses and the procedures used to test these hypotheses are also provided. The results of these statistical tests are presented in Chapter IV. Analysis and discussion of the results are also included.

Chapter V summarizes the major results of these investigations and draws conclusions concerning the impact of system variables, the overall efficiency of buffering strategies, and the most appropriate strategy to buffer the system against supply uncertainty. Finally, a suggestion is made to extend the current research to more system variables.

CHAPTER II

REVIEW OF THE LITERATURE

There has been little empirical research on how to protect manufactured parts, components, subassemblies, or final assemblies against demand and supply uncertainties.

MRP advocates do not agree whether safety stock should be used in MRP. Those who oppose the use of safety stock in MRP argue that because MRP systems adapt to changing conditions that affect demand and lead times, safety stock will not actually be used under the vast majority of circumstances in MRP (23). Orlicky (43, p. 79) argues that an item safety stock forces the MRP system to overstate requirements which is undesirable and sometimes leads to distorted timing when the safety stock causes the net requirement to be pulled forward in time. This overstated requirement or false timing tends to cause confusion, unnecessary expense, and loss of credibility in the MRP system. Wight (59, p. 34) stated that an objective of MRP is to plan priorities effectively and safety stock tends to dilute priorities. Their message is clear: safety stock should have very limited role in MRP systems, appearing only at the finished product level or for items whose demand is not strictly derived from production schedules. Peterson and Silver (45, p. 474) also believe that it is more effective to avoid shortages and excess inventories through the adjustment of production lead times, these adjustments being accomplished by expediting or, more generally, shifting priorities of shop orders.

Outright elimination of any buffering policy for dependent demand items may not be the final answer in MRP. New (41) indicated that operating an MRP system on the basis of zero buffer stocks might cause

some problems because of variations caused by uncertainty of demand and uncertainty of supply, both in terms of time and quantity, in the system. He also added that correction of actual stock errors elsewhere in the system as another cause of these variations. Stressing supply uncertainty, Buffa (10, p. 334) mentioned that buffer stock is required to absorb variations in supply schedule. He indicated that the time required for processing orders through an intermittent system is variable because of such factors as delays and breakdowns. Moreover, the actual quantity delivered from production is variable because of the scrap. Orlicky (43, p. 80) himself did not rule out completely the possibility of using safety stock under an MRP system. He stated that there is justification for carrying some safety stock of an item where the resupply performance is erratic and uncontrollable.

If timing and quantity supply uncertainty is inevitable for some items under MRP system, the question becomes: What is the best way to buffer the system against this uncertainty?

Safety stock is commonly used in the case of stock replenishment (independent demand systems) as a way of absorbing variations in demand and lead time. Under these systems, the reorder level is set to cover normal usage during the supply lead time plus the safety stock. Safety stock is computed on the basis of a demand distribution during the supply lead time for the item in question and the desired service level (see 8, 17, 25, 33, 61). Hadley and Whitin (26) in an early work, discussed most procedures available for developing safety stocks under conditions of known and unknown stockout cost for discrete and continuous demand distributions. These procedures are designed mainly for independent demand items.

As with the stock replenishment system, Plossl and Wight (59) stated that safety stocks are necessary also in material requirements planning to protect against demand variations for the end products and supply variations for components. They have discussed the available procedures and pointed to the need for more theoretical work to be done on developing a rational basis for setting safety stock levels.

Moore (39) discussed the use of safety stock with MRP. He explained the similarity between MRP and the two basic systems of inventory replenishment, fixed order and periodic ordering, to justify using the same methods in establishing safety stocks in both MRP and the other inventory systems. However, for an end-item with independent demand, under MRP, safety stock calculations must consider the cumulative lead time (CLT) for the item if its components are manufactured or purchased in discrete quantities dictated by higher level use. Failing to do so, as he said, will cause customer service to fall short of the desired goal, or priority changes, and/or emergency orders will be caused when the user attempts to replenish the safety stock at less than the cumulative lead time. His suggested system is simple: Calculate safety stock according to the maximum usage during the cumulative lead time and a desired service level, use safety stock to satisfy the surge in demand, replenish the safety stock at the cumulative lead time for the item.

Eichert (19) addressed the problem of demand uncertainty under MRP systems in a very special way. He suggested that most unplanned demand and master schedule errors may be treated as an independent requirement. These "other requirements" are field failures, non-productive demand, shop failures, rejected materials, vendor shortages, change notices, engineering changes, data errors, and pull-ins. He introduced a technique

which may be applied as part of a material requirement planning system to account for these requirements. Field failure, non-productive demands, and pull-ins can be included in the master schedule by separate forecasts for each. Shop failures, rejected material, and vendor shortages can be predicted by determining the failure, rejection, or shortage rates for parts or vendors. On the other hand he recognized the difficulties of attacking change notices, engineering changes, and data errors. This practical approach of a separate forecast for each "other requirement", protects the system against uncertainty through the application of statistical inventory techniques to unexpected requirements.

New (41) pioneered the research on introducing safety factors into requirements plans. He discussed three methods available to protect the system against both supply and demand uncertainty. These are: fixed quantity buffers, safety times, and increased master production schedule. He pointed out some of the pitfalls associated with these methods. Fixed quantity buffer requires the implementation of a fairly complex system of checks to insure that buffer stock usage and replenishment are planned correctly. On the other hand, safety time as a buffer inflates both the length of the planning horizon required and the total composite lead time for a multi-level assembly. As for increasing the requirements forecasts used in the master schedule in terms of "scrap" or "yield loss" allowances, he indicated that it is superfluous when used at the finished item stage. Part of the reason for the buffer stock is to absorb such variation in production yield. Using these allowances for lower level components is also fairly critical to the performance of the system.

In an effort to offer some guidance in selecting an appropriate procedure, he concluded that particular procedures are appropriate only under specific circumstances. The safety time system is recommended on sparse schedules--lumpy demand--where production is infrequent, and also at the raw material level when items are purchased from outside the company. When using safety time, the projected stock vary widely from period to period. Therefore, when production is infrequent the safety time system adjusts much more quickly to scheduled production than would a fixed quantity buffer stock. Using the latter system under these circumstances means that the buffer quantity held all the time when only few orders per year will be made. On the other hand, using buffer stock at the finished item stage is appropriate. Using safety time in this case with its projected stock variations represents an uncertain level of "safety cover" for the schedule over time. Moreover, he suggested that combinations of methods be used under different circumstances. A safety time system may be used for raw materials and a fixed buffer for intermediate items in a company manufacturing for "call-off" schedules, while a company manufacturing solely for sales from finished stock might hold a fixed buffer at the highest level and a safety time for lower level items. Though this article does not offer any experimental results or any clear relationship between uncertainty types and levels, and different buffering factors, New does provide a theoretical basis for studying this problem.

Whybark and Williams (38) pioneered the experimental research on material planning under uncertainty. They disagree with the idea that safety stock should have a limited role in MRP systems. This position, as they said, assumed that sufficient production capacity and/or

flexibility exists to absorb the results of changes that can occur when the MRP system is rerun each period. They argue that at some point this flexibility may not be sufficient.

In their study, uncertainty was categorized into four different categories: demand timing uncertainty, supply timing uncertainty, demand quantity uncertainty, and supply quantity uncertainty. The level of quantity uncertainty was measured by the standard deviation of the difference between projected inventory balance and actual inventory balance. Demand quantity uncertainty was measured in terms of the coefficient of variation of an item's gross requirement. A uniform distribution, of the actual requirements around the projected gross requirement each period, was used to generate actual requirements. Similarly, the actual quantity received was assumed to be uniformly distributed around the quantity scheduled to be received for each order. On the other hand, demand timing uncertainty was introduced by interchanging gross requirements between periods while the exact timing of order arrival was generated by varying the scheduled arrival time by as much as ± 2 periods. Their simulation analysis focused on evaluating two inventory oriented buffering techniques, safety stock and safety lead time, for a single component item under each category of uncertainty. The relationship between the actual service level and average inventory was the criterion used to test the hypothesis that there would be a "preference" for either safety lead time or safety stock under each of the categories of uncertainty. In order to test the effect of demand variability of the gross requirements and the level of uncertainty on the preference between the buffering techniques, three levels of coefficient of variation and uncertainty were provided for each of the four uncertainty categories. They concluded that under conditions

of uncertainty in timing, safety lead time is preferred, while safety stock is preferred under conditions of quantity uncertainty. After a number of validation runs, they concluded also that these effects did not change with the source of uncertainty (demand or supply), lot sizing technique, lead time, average demand level, uncertainty level, or coefficient of variation in their study. The study also indicated that as the coefficient of variation and uncertainty level increase, the importance of making the correct choice between safety stock and safety lead time increases.

This study represents a required step toward understanding the effect of uncertainty in MRP system. It provides a description of the behavior of a single part under different uncertainty conditions, which is a basis for understanding the whole system. It also provides a general guideline for choosing between the two buffering techniques: safety stock and safety lead time. However, it is difficult to generalize their results to any part when considering a multi-stage production-inventory system. Under such a system some additional factors must be considered. Some of these factors are the interaction of the buffering techniques, the different combinations of uncertainty environments, the different "joint" buffering techniques, and the performance of the whole system. This study also made no determination of how much safety stock or safety lead time should be used.

Banerjee (1) has studied the selection of different buffering techniques in an MRP system. He investigated several safety stock policies. The first policy has safety stocks provided for the finished products based on forecast error. The second policy has safety stocks provided for the finished products based on forecast error and for the raw materials

based on supply uncertainty. The third policy has safety stocks provided at three levels with supply uncertainty buffered against at both intermediate and raw material levels. Although he claims that buffer inventories for the lower level items are automatically provided for during the process of product explosion and demand derivation at the lower levels, his first buffering technique turned out to be less efficient with a high stockout level according to his results. On the contrary, his results indicate that providing safety stocks for the finished products and raw materials turns out to be the best policy that considers all the uncertain input variables in the system. His conclusions, however, seem to support the conventional contention that safety must be provided only at the finished product and raw material levels if they should be allocated at different stages. Though his study is considered one of the few early empirical investigations of the problem of uncertainty in a multi-stage production environment, Banerjee used only demand uncertainty effect when calculating the required amounts of safety stock. This partially justifies not being able to generalize his results when supply uncertainty is considered. Moreover, the study was limited to only one buffering method, namely; providing safety stock, i.e. some other buffering methods, such as safety lead time, was not considered.

Callarman and Mabert (11) studied using material requirements planning systems with demand uncertainty. They provide a Service Level Decision Rule (SLDR) which might be used for estimating the amount of safety stock needed or the economic Time Between Orders (TBO) needed to gain a specified service level. This was done by mapping in a linear regression model service level performance against the independent variables of demand variation, forecast error, safety stock and TBO.

Then by solving this model once for safety stock or for TBO when safety stock equals zero, the two decision rules were developed. After testing the performance of the decision rules, they concluded that these decision rules do not give the exact amount of safety stock needed or the exact TBO needed to get the desired service levels. However, they give a good estimate of safety stock requirements to use as a starting point for further analysis.

Mehta (35) discussed how to handle safety stock in an MRP system. He explained some problems associated with deducting safety stock from on hand balance. He suggested another method in treating safety stock which may help to maintain valid priorities in the system. He recommended not to deduct safety stock from on hand balance, therefore making it available for use and to replenish safety stock in the very first period beyond aggregate lead time. In other words, companies must continuously use and plan safety stock.

Liaw (32) examined the effect of various safety stock policies in an MRP system that was subject to both demand and supply uncertainty. Nine different safety stock policies, derived from two heuristics, were studied. Heuristic A is based on the argument that total inventory risk can always be recognized by examining the difference between the actual requirement and the actual amount available for an end item. Therefore the required safety stock, for all items at any level, is a function of the average unforeseen inventory risk for the end items. This heuristic method resulted in three major safety stock policies. One is to install safety stock at the finished product level only. The second is to carry safety stock for work-in-process items only. The third is to

carry it for raw materials only. Heuristic B on the other hand, suggested that various inventory risks at different inventory stages be treated separately which results in a policy that provides safety stocks for all items at all stages. Four more strategies were derived from heuristic B. One of them is to provide safety stock at all three levels but equal weights are assigned to the three levels, while the other strategies are using the safety stock of only two of the three levels with arbitrarily assigned equal weights at each level. Two other independent variables were used in this study to represent different operating conditions, namely inventory risk (degree of uncertainty) and cost structure.

The results of his study indicated that both of the structural variables (inventory stock and cost structure) may affect the performance of a safety stock policy on five selected criterion variables: number of stockouts, number of outages, inventory carrying cost, total cost and return on investment. Moreover, it was found that the interaction effect between inventory risk and cost structure was significant. This was interpreted to mean that these two factors should be considered together, rather than independently, to make the best use of safety stocks in a multi-stage or multi-product production-inventory system using MRP. In terms of any preference pattern that might exist among the buffering strategies, his results partially support the conventional contention that buffer stocks can be carried at finished product level only. This is only recommended where there is considerable inventory uncertainty involved at this level and the unit values of the items at other levels are sufficiently high. Otherwise, the strategy that provides buffers at all three levels become more desirable especially when there are high uncertainties involved at the lower levels.

In spite of the fact that this study is one of the few to consider using safety stock in MRP in a multi-stage and multi-product production-inventory system, some limiting aspects of this study are (1) only one type of supply uncertainty was studied, that is, quantity uncertainty, i.e., invariability of lead times was assumed, and (2) only various safety stock policies were considered without considering some other buffering techniques, like safety lead time.

Summary and Conclusions

A rather extensive review of the literature concerning the problem of protecting a multi-stage production system using MRP against demand and supply uncertainty has been presented. From this literature survey it is apparent that further systematic study needs to be accomplished incorporating more characteristics of multi-stage production systems. In the case of using MRP system, most of the buffering research to date has been limited to (1) the use of safety stock as the only buffering technique without considering some other inventory buffering techniques, like safety lead time (1, 7, 32), (2) the use of different buffering techniques for only a single "part" rather than studying a multi-stage production system (58), (3) buffering the system against different conditions of demand uncertainty only without considering supply uncertainty (11), and (4) considering quantity uncertainty as the only type of uncertainty in the system (32). Although these studies represent a required contribution toward the understanding of this problem, conclusions concerning the use of inventory buffering strategies under different types and levels of uncertainty in a multi-stage system have not been developed fully. This research hopefully adds to this body of knowledge.

A joint buffering strategy as used in this study is a combination of different buffering techniques (safety stock and safety lead time) applied to different levels of the product structure. Two different buffering techniques are used for purchased items level and in-process inventory level (this includes intermediate and end item levels) producing four buffering strategies. Two types of supply uncertainty, quantity and timing, are used at two levels, high and low, for each. Moreover, the idea of joint uncertainty is used in this study. It is a combination of different types and levels of supply uncertainty applied to different levels of the product structure. Therefore the performance of each buffering strategy is examined under different combinations of "joint" supply uncertainty. This point will be discussed in more depth in the next chapter dealing with experimental design.

CHAPTER III
RESEARCH METHODOLOGY

According to the research objectives described in Chapter I, and in light of the literature reviewed in Chapter II, additional aspects of the use of different buffering strategies in a multistage production system are explored in this research. In the case of multistage production system, multilevel conditions of supply uncertainty are relevant. Therefore the performance of the production system under different conditions of supply types and degrees of uncertainty is considered. Also, instead of applying a single buffering strategy at all levels of product structure, some proposed joint (multilevel) buffering strategies are evaluated.

Research Hypothesis

In order to investigate and study this problem a tentative set of null hypotheses of this research were developed:

Null Hypothesis No. 1 The buffering strategies (i.e., the joint buffering strategies defined earlier) have no effect on the system performance.

Null Hypothesis No. 2 Type of supply uncertainty has no effect on the system performance.

Null Hypothesis No. 3 Degree of supply uncertainty has no effect on the system performance.

Null Hypothesis No. 4 Type of supply uncertainty has no effect on the performance of the buffering strategies.

Null Hypothesis No. 5 Degree of supply uncertainty has no effect on the performance of the buffering strategies.

Null Hypothesis No. 6 No "preference" pattern exists for different buffering strategies.

System performance is measured using performance measures discussed in a later section of this chapter.

Experimental Design

In order to outline the experimental design to be adopted in this research, the various factors that are subject to experimental control and their levels are summarized in Table 3-1.

(1) Joint Buffering Strategies (B)

Two inventory oriented buffering techniques, safety stock (SS) and safety lead time (SLT), have been chosen to be examined in this study. The reason for selecting these techniques is two-fold. First, other techniques that rely on frequent MRP replanning and expediting assume that sufficient production capacity and/or flexibility exists. Sometimes this flexibility is not sufficient (58). There are some items where lead time actually is relatively fixed (42). Second, some of these selected techniques have been studied, to some extent, by previous researchers, therefore comparison of the results will be possible.

These selected buffering techniques are used, in conjunction with the product structure, to formulate the joint buffering strategies to be studied in this research. In order to reduce the potential number of combinations, the product structure levels were reduced to two. The "upper" level incorporates both end items and "intermediate" level items. The "lower" level includes raw materials and purchased items only. End items and intermediate components are made in-house, therefore they are similar from the view point of supply uncertainty. Because of the availability of information about production schedule and capacity

TABLE 3-1
SUMMARY OF EXPERIMENTAL FACTORS AND
THEIR CLASSIFICATIONS*

Factor	Classification	Description
Buffering Strategy (B)	1	SS/SS
	2	SS/SLT
	3	SLT/SLT
	4	SLT/SS
	5	O/O
	6	SS/O
Type of Supply Uncertainty (T)	1	Timing uncertainty for both levels: T/T
	2	Quantity uncertainty for both levels: Q/Q
	3	Joint uncertainty 1: T/Q
	4	Joint uncertainty 2: Q/T
Degree of Supply Uncertainty (D)	1	High uncertainty for both levels: H/H
	2	Low uncertainty for both levels: L/L
	3	Mixed uncertainty 1: H/L
	4	Mixed uncertainty 2: L/H

*where:

O: no buffering, SS: safety stock strategy, SLT: safety lead time strategy, T: timing uncertainty, Q: quantity uncertainty, H: high uncertainty, and L: low uncertainty.

conditions for the internally produced items, it is assumed that management is able to control the situation, to some extent. This is not the case for raw materials and purchased items because most of the uncertainty factors are controlled by the outside vendors.

By applying safety stock (SS) and safety lead time (SLT) at both "upper" and "lower" levels, four joint buffering strategies are formulated, namely: safety stock at both levels (SS/SS), safety stock at the "upper" level and safety lead time at the "lower" level (SS/SLT), safety lead time at the "upper" level and safety stock at the "lower level" (SLT/SS), and safety lead time at both levels (SLT/SLT). Two more buffering strategies are used: no buffering at both levels (0/0), and safety stock at the "upper" level and no buffering at "lower" level (SS/0). The 0/0 strategy is used to represent a base point for analyzing the results concerning the relative performance of different buffering strategies. The SS/0 strategy is necessary because it is frequently mentioned in the literature (39, 53) as the appropriate way to protect a production system against uncertainty. Figure 3.1 is an example of a joint buffering strategy.

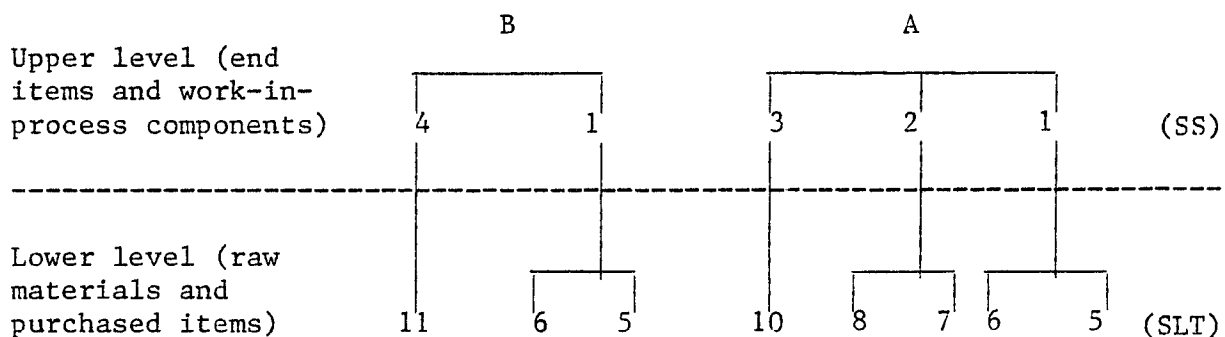


FIGURE 3.1

The procedure for determination of safety stock and safety lead times required for each level, is discussed in a later part of this chapter.

(2) Type of Supply Uncertainty (T)

Two different types of supply uncertainty are used in this study: Quantity uncertainty (Q), and Timing uncertainty (T). In conjunction with the "upper" and "lower" levels, four different combinations of supply uncertainty type are utilized. These include timing uncertainty at both levels (T/T), quantity uncertainty at both levels (Q/Q), timing uncertainty at the "upper" level and quantity uncertainty at the "lower" level (T/Q), and quantity uncertainty at the "upper" level and timing uncertainty at the "lower" level (Q/T). For "lower" level items, supply quantity uncertainty arises when suppliers deliver amounts other than that ordered; i.e., actual receipts are not equal to scheduled receipts because of excess supply or supply shortages. On the other hand, supply timing uncertainty for "lower" level items arises from variations in vendor lead times. Deliveries from suppliers are not always made according to that promised because vendor lead time is a function of many uncontrollable factors (50).

"Upper" level items are also subject to both quantity and timing uncertainty. When production lots incur scrap losses or when there are shortages of lower level materials, the actual receipts will vary from the amount scheduled. Delays, breakdowns, or a change in plan, on the other hand, may cause a variation in the manufacturing lead time for internally supplied items. Moghaddam and Bimmerle (38) reported nineteen factors influencing manufacturing lead time, most of them are of a probabilistic nature. Though his study was under independent demand environment, Vinson (55) indicated that lead time unreliability (variability of lead time from mean lead time) is of greater importance than either the mean lead time or the variability of demand in explaining inventory cost behavior.

In this study, quantity uncertainty is introduced through considering the scheduled receipt as the mean quantity to be received for each item, and the actual receipts is distributed about this mean according to exponential distribution and degree of uncertainty. Similarly, the actual lead time is distributed about the projected lead time according to the Poisson distribution.

(3) Degree of Supply Uncertainty (D)

Two levels of supply uncertainty are used in this study: low (L) and high (H) uncertainty. A large mean shortage (λ) is used in the exponential distribution to generate the high quantity uncertainty situation. Low quantity supply uncertainty is associated with a $\lambda_1 = .1$, and high quantity supply uncertainty is associated with a $\lambda_2 = .3$. On the other hand, low timing supply uncertainty is associated with a mean delay $\lambda'_1 = .1$ while high timing supply uncertainty is associated with a $\lambda'_2 = 1$.

These two selected levels of uncertainty, for both quantity and timing, are used for both low level and high level items. In conjunction with the product structure, they are used to formulate the four multilevel combinations of the uncertainty degree that are studied in this research. They are high uncertainty at both levels (H/H), low uncertainty at both levels (L/L), high uncertainty at the "upper" level and low uncertainty at the "lower" level (H/L), and low uncertainty at the "upper" level and high uncertainty at the "lower" level (L/H).

The process of introducing different uncertainty levels in the system will be explained in detail during the discussion about operation of the simulation model in the last section.

Statistical Procedures

To observe any possible main and interaction effects of all three factors, a full factorial experiment of dimension $4 \times 4 \times 6 = 96$ will be

adopted. Factorial experimentation is highly efficient because every observation supplies information about all the factors included in the experiment. Secondly, it is a method of investigating the relationship between the effects of different factors (35). The Three-Factor Classification model chosen to represent this experiment is (28):

$$\begin{aligned}
 Y_{ijk\ell} &= \mu + \alpha_i + \beta_j + (\alpha\beta)_{ij} + \gamma_k + (\alpha\gamma)_{ik} \\
 &\quad + (\beta\gamma)_{jk} + (\alpha\beta\gamma)_{ijk} + \epsilon_{ijk\ell}, \\
 \epsilon_{ijk\ell} &\sim N(0, \sigma^2) \text{ indep.} \\
 i &= 1, \dots, 6 \\
 j &= k = 1, \dots, 4 \\
 \ell &= 1, \dots, n
 \end{aligned}$$

where

- μ is the true mean effect,
- α_i is the true effect of the i th level of factor (B),
- β_j is the true effect of the j th level of factor (T),
- γ_k is the true effect of the k th level of factor (D),
- $(\alpha\beta)_{ij}$ is the true interaction of the i th level of factor (B) with the j th level of factor (T),
- $(\alpha\gamma)_{ik}$ is the true interaction of the i th level of factor (B) with the k th level of factor (D),
- $(\beta\gamma)_{jk}$ is the true interaction of the j th level of factor (T) with the k th level of factor (D),
- $(\alpha\beta\gamma)_{ijk}$ is the true interaction of the i th level of factor (B) with the j th level of factor (T) and the k th level of factor (D), and
- $(\epsilon_{ijk\ell})$ is the error associated with the ℓ th experimental unit subjected to the ijk^{th} treatment combination.

n = number of replications.

Though the three-way interaction $(\alpha\beta\gamma)_{ijk}$ is a part of this statistical model, it is not considered in this analysis. Most of the time it has very little meaning and is rarely tested (24). Figure 3.2 depicts the experimental design for this study.

		H/H				L/L				H/L				L/H			
		T/T	Q/Q	T/Q	Q/T	T/T	Q/Q	T/Q	Q/T	T/T	Q/Q	T/Q	Q/T	T/T	Q/Q	T/Q	Q/T
Buffering Strategy (B)	1	SS/SS															
	2	SS/SLT															
	3	SLT/SLT															
	4	SLT/SS															
	5	O/O															
	6	SS/O															

FIGURE 3.2 THE EXPERIMENTAL DESIGN

In this study, all studied factors are considered fixed variables. Therefore the statistical model is treated as fixed effect model. This point will be clear in the statistical analysis section.

In this model, it is assumed that the same number of replications unit exists for all runs (treatments). The way this required number of replications was estimated is reported in the next section.

Number of Replications (Sample Size)

The number of replications (n) necessary to detect a difference (d) between means in the analysis of variance was estimated using the power approach. This approach permits controlling the risks of making both Type I and Type II errors. Feldt and Mohmoud charts (40, p. 493) are available to furnish the appropriate sample size directly. They are applicable only when all factors levels are to have equal sample sizes, which is the case in this study.

In order to be able to use these charts the following specifications were made:

1. A level of $\alpha = .05$, at which the risk of making a Type I error is to be set, is adapted for this study.
2. The value of a noncentrality parameter ϕ' at which the risk of making a Type II error is to be controlled is estimated as follows:

$$\phi' = \frac{d}{\sigma} \sqrt{\frac{1}{2r}}, \text{ where}$$

d the maximum difference between pairs of level means for which it is important to recognize differences in the population means,
 σ the standard deviation of the considered performance measure,

r number of levels of the considered factor. In this study r equals 5, 4 and 4 for factors B, D and T, respectively. A value of $r = 5$ is used as an average for the number of levels. This implies that ϕ' will equal $(.316)d/\sigma$ for all d/σ ratios. Table 3.2 is constructed to give the value of n required in terms of the ratio d/σ .

Six preliminary runs were conducted to estimate d and σ for selected performance measures. Table 3.3 presents the results of these primary runs. Table 3.3, in conjunction with Table 3.2, indicates that five replications are statistically sufficient. Therefore, five independent simulation runs were conducted for each cell. Throughout the study a reestimation of d and σ was done and the new values were used to recalculate the required number of replications. This precaution step was required to assure that the sample size used, five in this case, was always statistically adequate throughout the study. Table 3.3 includes also the overall estimates for d and σ for different performance measures. All new estimates support the initial conclusion that five replications are required. This implies that the power of the F-test is still above .90 whatever the performance measure being analyzed.

The Statistical Analysis

The final step in the procedure for conducting a simulation experiment involves the analysis of the data generated by the computer from the model of the simulated system. A number of alternative forms of analysis have been suggested (36). Among these, the analysis of variance and a multiple comparison procedure is utilized in this study.

Analysis of variance, in conjunction with an appropriate experimental design, has the capability of investigating the effects of several factors at once. It is frequently used in inventory simulation research (57),

TABLE 3.2

The Number of Replications Required in Terms
of the Ratio d/σ

$$\alpha = .05, \beta = .1, r = 5$$

d/σ	ϕ'^*	n
.25	.079	**
.50	.158	**
.75	.237	65
1.00	.316	35
1.25	.395	22
1.50	.474	18
1.75	.553	12
2.00	.632	10
2.25	.711	8
2.50	.790	7
2.75	.869	5

$$*\phi' = (.316)(d/\sigma)$$

**Values could not be found from Felt and Mahmoud's Charts

TABLE 3.3
Data Used to Calculate the
Required Number of Replications

Performance Measure		Maximum Level Mean	Minimum Level Mean	d	σ	d/ σ
HOLC	Prim.*	6879366.	25199798.	4359568.	926232.06	4.7067
	Study**	7949235.	2995972.	4953263.	1173551.26	4.2207
INVC	Prim.	7538398.	4003928.	3534470.	97599.54	3.6214
	Study	9218996.	5267181.	3951815.	1173511.51	3.3675
TOC	Prim.	7754654.	4173185.	3581469.	774405.16	4.6248
	Study	9262146.	4414284.	4847862.	12554744.44	3.8613
BO	Prim.	11817	1498	10319	1317.20	7.8340
	Study	9215	1819	7396	622.06	11.8902
STK	Prim.	107	14	93	15.39	6.0421
	Study	78	12	66	8.21	8.0036
SLVL	Prim.	.971192	.772750	.198442	.02382	8.3245
	Study	.965032	.821629	.143402	.012081	11.9323

* Prim.: data are taken from the six preliminary runs with 25 observations each.

** Study: data are taken from the overall simulation experiment (96 runs with five observations each).

and it has been reported that it is useful in all simulation studies where the analyst may wish to alter a variety of factors in the model to determine the ones which have a significant effect on performance of the model (36).

However, this procedure requires a number of assumptions, i.e., independent of observations, normality of populations and homogeneity of variance for each treatment and experimental unit (44). In this study, using the independent replications methods, as will be explained, assures the requirement of independence to be fulfilled. On the other hand, it has been reported that moderate departures from the assumptions of normality and homoscedasticity is not a critically important matter (14). Neter and Wasserman (40) state that the point estimators of factor level means and contrasts are unbiased whether or not the populations are normal. Moreover, the F-test for the equality of factor level means is little affected by lack of normality, either in terms of the level of significance or power of the test. They also indicate that the F-test is robust against unequal variances if the sample sizes are equal.

The F-tests, in the context of analysis of variance, will be used to indicate whether or not significant main and interaction effects of the studied factors exist. If the F-test leads to the conclusion that the factor level means are equal, the implication is that there is no relation between the factor and the performance measure. On the other hand, if the F-test leads to the conclusion that the factor level means differ, the implication is that there is a relation between the factor and the performance measure and a different procedure must be used to answer the question of how these factor level means differ.

Several procedures are available to examine how the different factor levels compare with one another in terms of the system performance measurement (14, 40, 52). The Tukey method of multiple comparisons is utilized in this research. This procedure is considered appropriate in this study because all factor level sample sizes are equal for most dependent variables (six out of seven), and only all pairwise comparisons of factor level means are of interest in this study. However, conditions of normality of populations and homogeneity of variance must be fulfilled before using this method. Testing for these two conditions is reported in the next chapter.

Performance Measures

The criterion performance measures that will be used in this research are:

- (1) Total inventory carrying cost for items at all three levels in the system (HOLC),
- (2) Total setup and carrying costs (INVC),
- (3) Total cost (TOC) (sum of the setup, carrying, overtime, and stockout costs),
- (4) Total number of units short (BO),
- (5) Total number of stockout occasions (STK),
- (6) Service level (SLVL) for the finished products, which measures the percent of the amount of the scheduled requirements of the finished products that were met during the planning horizon,
- (7) Buffering Cost Effectiveness Measure (BCEM), this criterion measures the proportionate increase in the service level resulting from each increment in inventory cost. This performance measure seems to give more insight into the overall economical effect of a particular buffering

strategy. BCEM was calculated in this study as follows:

$$\text{BCEM for strategy } i = \frac{\Delta \text{ shortages}/(\text{shortages})_{0/0}}{\Delta \text{ inventory cost}}$$

where:

Δ shortages: the amount of decrease in the finished products shortages (performance measure 4) resulting from buffering strategy i , and calculated by subtracting number of shortages of each buffering strategy from number of shortages of buffering strategy 5 (No buffering at both levels).

$(\text{shortages})_{0/0}$: number of shortages when "no-buffering" strategy is used. This value was the base for estimating (Δ shortages).

Δ inventory cost: the extra inventory cost required to implement buffering strategy i , and measured by subtracting inventory cost of "no-buffering" strategy from inventory cost of each other buffering strategy.

Some of these measures are used directly for testing research hypothesis. Likewise several combinations of some of these measures help in explaining the results.

Simulation Model

A simulation model is considered a valid research vehicle for exploring MRP system performance (4). Therefore, this study was conducted using a simulation model to represent a multilevel production system. Some versions of this model have been used by previous researchers (5, 6, 31, 49). A version was modified incorporating the main features of this study.

The simulated factory consists of two departments: Final Assembly and Subassembly. There are three types of inventory: finished goods, subassemblies, and raw materials. Raw materials are ordered from suppliers, and sales of finished products are made to customers. There is no outside demand for subassemblies. A general schematic diagram of the system and the physical flows within it are presented in Figure 3.3.

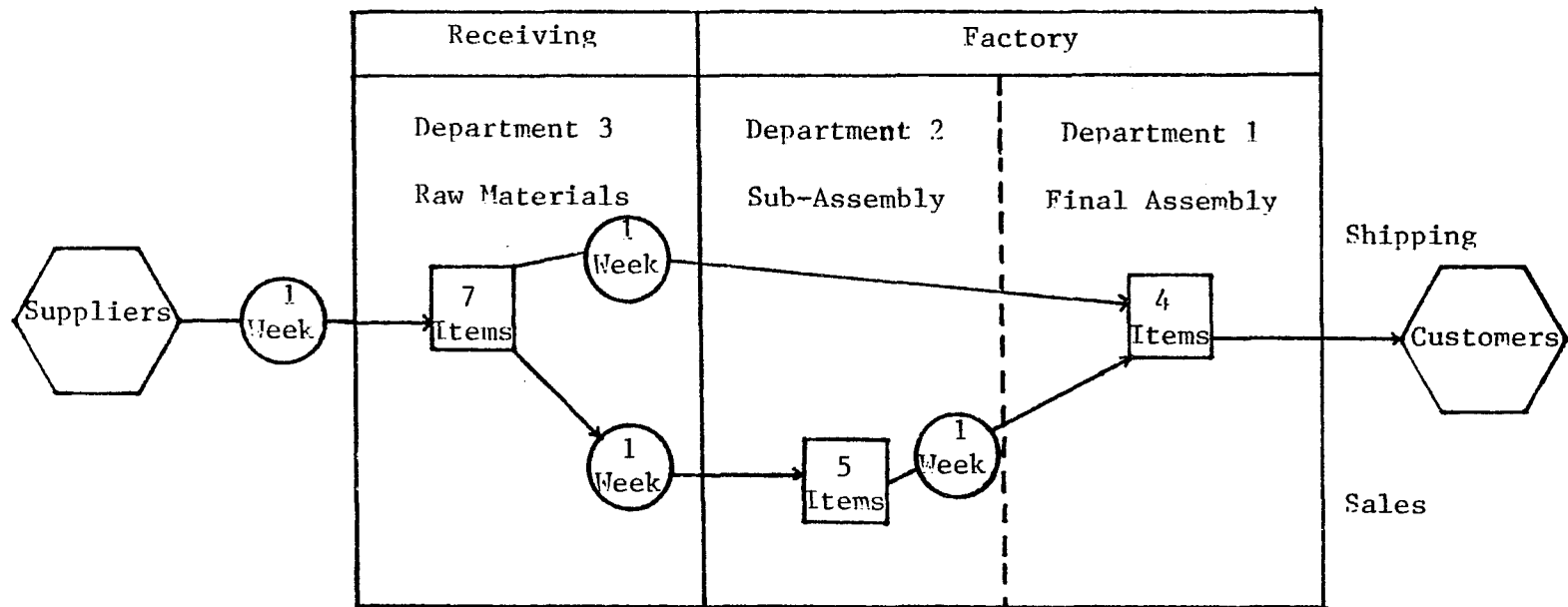


FIGURE 3.3, Schematic of Factory Organization and Work Flow

In each of the two departments, finished goods and subassemblies, there exists a machine group with adequate capacity to process the entire production plan in each period (unlimited capacity). Each department requires the same type of labor skills therefore, labor is perfectly transferable within each department. However, due to differences in skills required, workers cannot be transferred from one department to another. Limited overtime capacity, 30% of regular time capacity, is available in each department and desired production is automatically reduced if the limit is exceeded. Several more assumptions are made in this study. End-item demand is assumed to be deterministic (a perfect forecast), no production smoothing, and a lot for lot ordering strategy is used throughout the experiment.

The factory manufactures five end products, each calling for different assembly groups. Appendix (D) contains the product structure that shows the materials (raw materials, subassemblies) required to make subassemblies and finished products. This bill of materials includes 4 end items, 5 subassembly items, and 7 raw material items. Appendix (D) also includes the inventory file consisting of inventory on hand, setup time, run time per unit, lead time, setup cost per order, inventory value per unit, holding cost per unit, and any scheduled receipts for each item. A list of some other required initial conditions is also given in the appendix. One of these initial conditions is the gross requirements for each end item. It is assumed to be deterministic and available for the master production schedule at the initialization phase of this simulation.

The time unit used in this simulation is the week. Data about the performance of the system are collected for a planning horizon of fifty

two weeks. Tocher (37) suggested a very practical way to approach the problem of the run length. He suggested that the longest cycle in the plant should have been executed at least three or four times. The longest cycle, which is called the frozen period by Liaw (32) and the longest assembly "path" by New (41), in this research according to the selected product structure and the expected lead time value does not exceed 12 weeks. Therefore a simulated horizon of fifty two weeks is long enough to execute the whole assembly process four times at least.

Operating the Simulation Model

A computer simulation model of the period-by-period transactions is used in this study. The operating logic of this model is as follows: at the beginning of each period, the projected gross requirements for each end item, and all the required initial conditions, including the updated inventory files, is available. According to the selected buffering strategy, this information is used with the MRP logic to complete the explosion and generate requirements and orders for each item. If an order is required, it is scheduled for receipt in the appropriate future period according to the projected lead time. Next, delivery shortages and expected delays during this period are generated in order to assess the supply uncertainty in the system. One of the different sixteen categories of supply uncertainty combinations studied in this research is used. Actual receipts and production lots are released for possible processing during the execution phase. If the requirements are available, a lot is completed and made available as input to the next higher stage as of the beginning of the next period. In the case of final products, the lot is made available to meet external demand in the next period. In the event of material shortage, the system is asked to use

the available safety stock, if any. If the safety stock is not available, desired production is reduced proportionately in an attempt to just use up the available supply of the short material. Make-to-stock environments are assumed in the simulated model. This means that customers will not tolerate backorders, and failure to provide product on demand results in a lost sale and potential customer dissatisfaction. By the end of the period, records are updated according to the actual production and used as the basis for determining the requirement plan in the next period. This process is repeated for all periods during the simulated planning period. During the operation of the system, various statistics are collected to test the stated hypothesis. A diagram describing the simulation procedure is provided in Figure 3.4.

Initial Conditions and the Autocorrelation Problem

Before experimentation could begin, two issues had to be resolved: initial conditions and the autocorrelation problem. In this section, the criteria and data used to make decisions on both of these matters are presented.

Initial Conditions and Elimination of Transients. The problem of determining how to start the model, and how to obtain measurements that are not biased by the initial conditions are among the most difficult procedural questions in simulation (16). In many simulations, as in this research, the measurements that are to be made must take place when the system has reached equilibrium or steady-state conditions, that is, when the state of the system does not depend on the time when it is viewed (time independent). Conway (16, p. 48) points out, however, that "equilibrium is a limiting condition which may be approached but actually never attained."

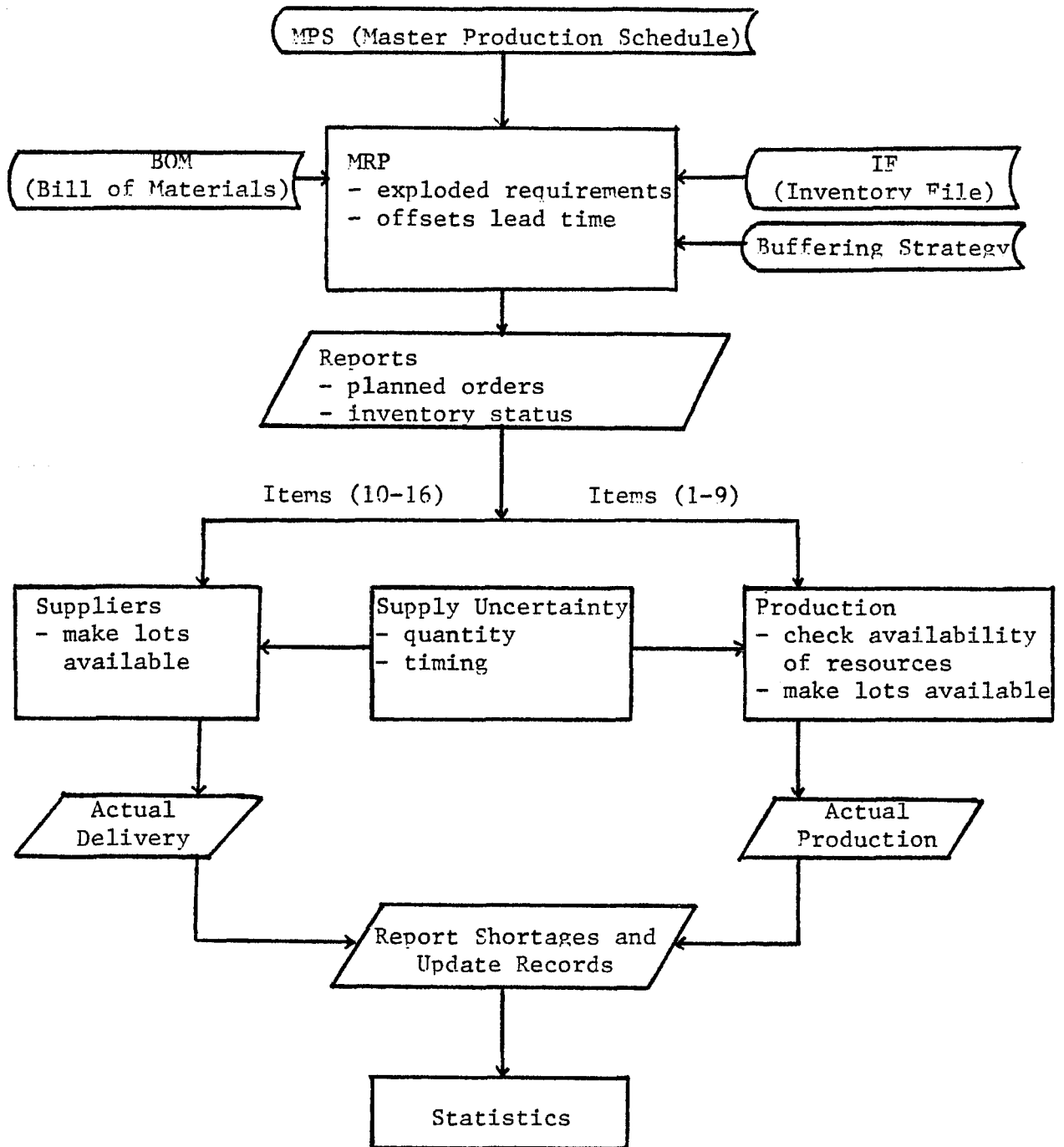


FIGURE 3.4 Elements of the Simulated System

Because of the selected initial conditions, a simulation run has a transient period when the state of the system is time dependent. During this period measurements of system behavior should not be taken since they could bias the results. To avoid this bias, this simulation had a "warm-up" or non-recording period prior to collecting measurements. At the end of this period the statistical accumulators were zeroed out, while the state of the system was left unchanged. From this point in the simulation, the system was considered to be in equilibrium.

The determination of the "warm-up" period length is subject to debate (30, 60), however, this length depends on the initial starting conditions of the model. Two basic strategies exist for setting starting conditions, one is to start with the system in the "empty and idle" state. Though it is easy to start the simulator under these conditions, the transient period is likely to be quite long (20). Under the second strategy, which was adopted in this research, the stabilization process can be accelerated by the choice of starting conditions that approximate the steady-state conditions of the system. Use of this alternative should reduce the transient period but in some cases, however, appropriate starting conditions may not be known in advance (56). In order to attack this problem in this research, three different sets of initial conditions were tried in twelve pilot runs to determine the effects each of it has on the behavior of the model. These pilot runs were selected to represent all combinations of supply uncertainty type (four cases) but under only the high degree of uncertainty condition. It was assumed that the variation of any of the performance measure throughout the study could not be greater than the variation detected under the high uncertainty

case in these pilot runs. The three initial inventory values that were used are : (a) no initial inventory, (b) one-half period demand initial inventory, and (c) one-period demand initial inventory, for each item. By plotting key system performance measures against time, it was clear that (b) comprises a set that reduced the duration of the "warm-up" period. Appendix (D) includes the initial inventory values used in this study. This set was used for each replication under the same uncertainty condition and buffering strategy. Moreover, it was used for all simulation runs in order to be able to compare one version of the model with any other version. This eliminated any distortion effects caused by difference in starting conditions (36). A non-recording period was also used in some cases to avoid any wild variation of any of the performance measurement at the beginning of the simulation. Because of the careful selection of the initial inventory levels, a four-week period was enough as a non-recording period in most cases.

Data Collecting and the Autocorrelation Problem. Another source of difficulty in the analysis of simulated data is that the output from simulation models is often autocorrelated (27, 56). In order to be able to use the classical analysis of variance techniques some steps must be taken to ensure the independence of the observations. The independent replications and the batch method are among the common approaches that could be used in this situation (22).

The independent replications approach requires repeating the simulation a number of times with all conditions the same except for the random number stream used to generate random events. Hence, the performance measures from each replication are taken as independent observations. Each one can then be used in estimating a variance for that performance measure.

The batch method involves breaking a simulation run into a number of separate periods or batches. System performance measures are then recorded for each batch. The objective is to have each performance measure in each batch be an independent observation from every other batch. The interrupt block approach to data collection is often used to achieve this goal.

Replicating runs is inefficient in that the wasteful starting transients are repeated in each replication (20). However, if the transient period is short because of using the appropriate set of initial conditions, the independent replicating method has the advantage of simplicity and guarantees independency of observations.

In this research, the independent replications approach is adopted. A run of the model for fifty two weeks is treated as one observation with regard to the aggregate statistics of operation of the system, that is, a run would yield one observation for such quantities as total inventory cost and total number of stockouts for the finished products. Because of the stochastic elements, aggregate performance measures vary from run to run when different random number sequences are used. A sample of size n is obtained by making n runs of a model starting from the same initial conditions but using a different random number sequence in each.

As indicated above, introducing different uncertainty types and levels, and using different buffering strategies are key factors in this research. Therefore, this last section explains in detail the process of generating different uncertainty environments and how safety stock and safety lead time are estimated in this study.

Supply Quantity Uncertainty Levels

Two categories of distributions can be used for simulations: empirically-derived distributions and theoretical frequency distributions (13). Because of the lack of any empirical approximation for both the actual delivery of raw materials and purchased items, and the actual production rate for end items and intermediate components, a hypothetical probability distribution is used in this study.

Whybark and Williams (58) used a continuous uniform distribution of the actual requirements around the projected gross requirement to represent the delivery process. Accordingly, in their study, there was an equal likelihood of receiving more or less than the planned (or expected) order receipts. Receiving more than the ordered amount is probably not typically encountered in most materials management systems. This would simply cause higher inventory costs unless the extra amount is offered with a considerable discount price which justifies accepting it.

In his study, Liaw (32) used normal random numbers to approximate the "percentage receipt failure" for each assembly and the shortage data for each raw material item. Since very few actual receipts are greatly below their expected amounts, the exponential distribution seems appropriate to model the distribution of the deviation between planned orders receipts and the amount actually received for raw materials and assembly items.

As used in this research, the distribution depends on a single parameter (λ) which represents the average percentage shortage (APS). For each item, APS represents the expected percentage shortage for each order and desired as:

$$\text{APS} = \frac{\text{Planned Order Receipts} - \text{Actual Order Receipts}}{\text{Planned Order Receipts}}$$

A larger APS represents higher risk of the production process or raw material supply being short. Low quantity supply uncertainty is associated with a $\lambda = \text{APS} = .10$, while high quantity supply uncertainty is associated with a $\lambda = \text{APS} = .30$; i.e., the average shortage, as a percentage of the planned order receipts in the case of high uncertainty is expected to be three times as much as the shortage percentage in the low uncertainty case. Figure 3.5 represents the two cases of quantity uncertainty used in this study.

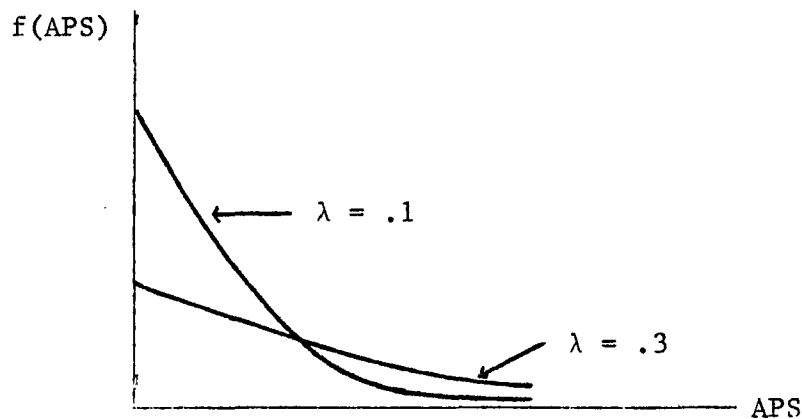


FIGURE 3.5 Quantity Uncertainty Levels

The procedure used for generating a random actual receipt for a particular order is as follows:

1. generate a standard uniform number, this will be a fraction, i.e., $0 \leq x < 1$,
2. transfer this number into an exponentially distributed number according to the specified level of λ . This value represents the APS for this order,
3. calculate the actual receipt for this order by using

$$\text{Actual Order Receipt} = (1 - \text{APS})(\text{Planned Order Receipts})$$

It is clear from the last formula, because APS is a positive fraction, that the actual receipts will always be less than or equal to the planned

receipts, i.e., only the case of shortage in delivery is considered in this research.

These procedures were used to generate the percentage receipt shortage for each assembly and subassembly and also for each raw material item.

Supply Timing Uncertainty Levels

One of the reasons lead time variability is not adequately studied in inventory theory is the fact that variation in lead time may not fit familiar probability distribution and/or may shift around in a pattern (55). This explains, to some extent, why some researchers (34, 53) discussed how to deal with lead time variation without specifying any particular theoretical frequency distribution to represent actual lead time. Some others (29) created their own hypothetical distributions. Liaw (32) assumed in his study a deterministic zero lead time for all items. In practical situations this is simply not realistic. Whybark and Williams (58) used ± 1 and ± 2 delay periods to represent low and high timing uncertainty respectively. Therefore, an early arrival of the order was possible in their study.

A Poisson probability distribution is used in this study to approximate the amount of delay. Accordingly, this delay is always zero or a positive integer value. The reason for selecting this type of distribution is two-fold. First, receiving an order before its due date is not typical of most real situations. Secondly, it seems more logical to assume that the typical supplier is attempting to meet his due date, only for a few times will he fail to do so. If this assumption is reasonable, as length of delivery delay increases, the associate probability of delivery delay decreases.

The average delay (λ') is used to represent the degree of uncertainty. Low timing supply uncertainty is associated with an average delay of $\lambda' = .2$ period while high timing uncertainty is associated with an average delay of $\lambda' = 1$ period. These two levels of λ' implies a risk of having any delay equal to about .18 and .63 respectively.*

The procedure used for generating a simulated actual lead time for a particular order will be accomplished by generating a Poisson distributed random variable according the values of λ' , then adding this value to the projected lead time to determine actual time of receiving an order:

$$\text{Actual Lead Time(ALT)} = \text{Planned Lead Time(PLT)} + \text{Generated Delay(GD)}$$

The Required Safety Stocks

Very little work has been done on any sort of "scientific" approach to the setting of the buffer stock levels (51). Banerjee and Saniga (3) introduced a procedure for determining appropriate safety stock levels for dependent demand inventory items. Starting with a particular end item demand distribution, normal or Poisson in their paper, they use the change of variable technique to obtain the probability distribution of the requirements for each dependent demand items. This estimated distribution is the basis for estimating safety stock for each item according to the desired service level. In addition to the complexity involved in the technique, a major drawback is that demand uncertainty is considered as the only reason for holding safety stock. While this

* If $\lambda' = .2$ $p(\text{delay} \leq 0) = .819$, therefore $p(\text{delay} \geq 1) = .181$.

If $\lambda' = 1$ $p(\text{delay} \leq 0) = .368$, therefore $p(\text{delay} \geq 1) = .632$.

might be accepted in replenishment systems, it is hard to ignore the effect of supply uncertainty when estimating the amount of safety stock for dependent demand inventory items. Callarman and Mabert (11) also ignored supply uncertainty when they introduced their Service Level Decision Rule (SLDR) as a way for determining the buffer stock. They treated safety stock as a function of the forecast error, coefficient of variation, and time between orders (TBO). All of these factors are of demand type.

In this research, because demand is assumed to be deterministic, supply uncertainty must be the base for estimating the safety factor for each item. Therefore, classical statistical techniques, with some modification, is used. The parameters of the statistical distribution selected to represent the shortage percentage, in conjunction with a desired service level, are used to estimate the required safety stock for each item. Consequently different levels of safety stock

At this point, it seems necessary to indicate that various supply uncertainties which take place at different inventory stages are treated separately. This is equivalent to heuristic B used by Liaw (32). The implication of this approach is that safety stock for finished products is provided to protect against production loss at final assemblies. Safety stock for intermediate items are provided to protect against production loss at the subassemblies, and safety stocks for raw materials are provided to protect against supply uncertainty, i.e., safety stock decisions are made only for the next lowest level.

The amount of safety stock (SS) required for each raw material item is estimated according to the value of λ , which represents the

uncertainty level, and the desired service level. The same service level must be used for all runs when estimating the safety stocks. A .95 service level is used in this study. Figure 3.6 represents the amount of safety stock required to satisfy this service level in the case of low and high uncertainty.

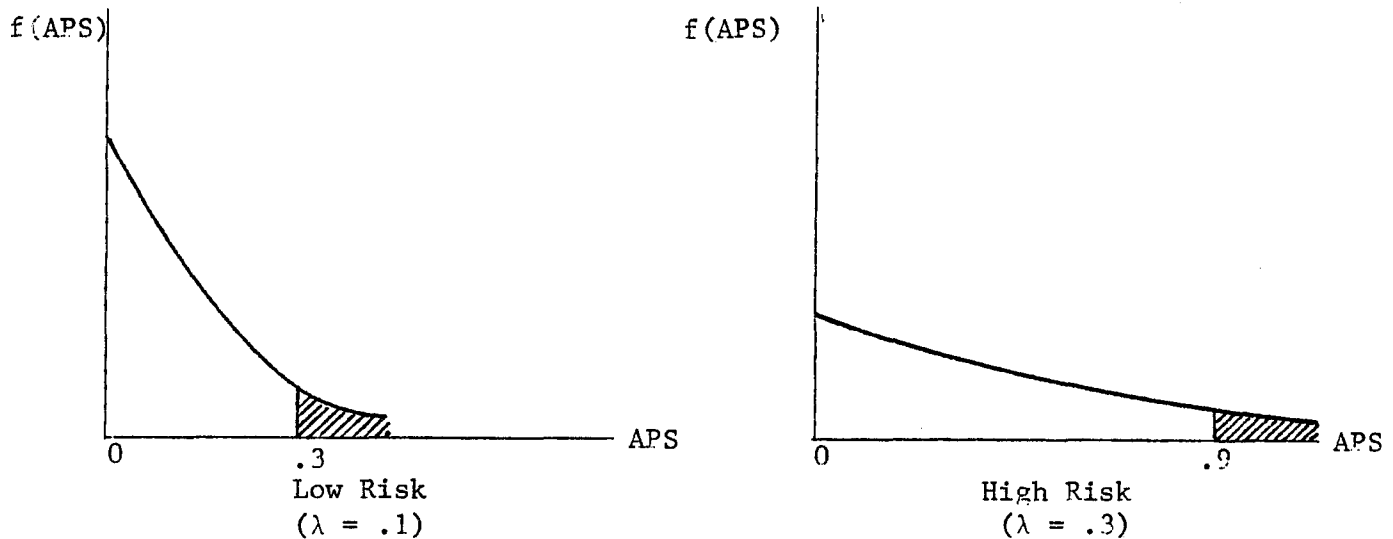


Figure 3.6

The above estimated values of APS are used directly to estimate SS as follows:

$$SS = \begin{cases} (\text{planned receipts}) (.3) & \text{if } \lambda = .1 \\ (\text{planned receipts}) (.9) & \text{if } \lambda = .3 \end{cases}$$

The amount of safety stocks required for each other intermediate and end items are estimated in the same manner except that the values .1 and .3 represents a production loss percentage rather than supply shortage percentage in the raw material case.

To incorporate these safety stock values in the simulated model, first a separate pilot run, for the total planning horizon, was conducted to calculate the planned receipts of all items, therefore all safety stock values could be estimated according to the formula indicated above. In each regular simulation run, these values are added to

the gross requirements to inflate the projected orders. As mentioned before, the system is asked to use these safety stocks when the need arises.

The Required Safety Lead Times

Safety lead time (SLT) implies a slight forward adjustment to the component order due date. The conventional statistical techniques are used in this study to estimate the required SLT for each item. A desired protection level against any change in the lead time of .98 is selected. This means a buffer lead time of one week must be used in the case of low timing uncertainty and three weeks must be used in the case of high timing uncertainty.*

Introducing safety lead time in the system is accomplished through moving the due date one or three weeks forward rather than increasing the lead time by the required amount of safety lead time.

*According to the Poisson distribution tables and the selected two level of λ' ,

$$p(x \leq \text{SLT}) = p(\text{delay} \leq \text{SLT}) = .982 \text{ when } \lambda' = .2, \text{ therefore SLT} = 1$$

$$p(x \leq \text{SLT}) = p(\text{delay} \leq \text{SLT}) = .981 \text{ when } \lambda' = 1, \text{ therefore SLT} = 3$$

CHAPTER IV
ANALYSIS OF DISCUSSION OF THE
EXPERIMENTAL RESULTS

The purpose of this chapter is to present and analyze the data generated from the simulation experiment that tested buffering strategy, type of supply uncertainty and degree of supply uncertainty hypotheses as outlined in the previous chapter. The results of these tests are presented and analyzed in the first section of this chapter. In a next section, comparisons of the performance of the different buffering strategies in each supply uncertainty category are presented and discussed. A general conclusion is then made in terms of the choice among various buffering strategies and some guidelines for selecting appropriate buffering strategies are provided in the last section.

Tests of Hypothesis

The analysis of variance (ANOVA) procedure was used to test the first five null hypotheses formulated in Chapter III concerning the main and interaction effects of the three factors on each of the response variables. Appendix A includes all analysis of variance (fixed effect model) results in Tables A.1 through A.7. These results are summarized in Table 4.1.

Although the F-test, used in ANOVA, is little affected by lack of normality and was reported to be robust against unequal variances, testing for normality of populations and homogeneity of variance was required before using Tukey's multiple comparison test. Normality was examined by the Kolmogorov-Smirnov test for all dependent variables, while Hartly's test was used to check for equality of variances. Results of these two procedures, as reported in Appendix B, seems to support the

TABLE 4.1
 SUMMARY OF ANALYSIS OF VARIANCE
 SIGNIFICANCE LEVELS OF FACTORS

Factors ^a		Performance Measures ^b						
		HOLC	INVC	TOC	BO	STK	SLVL	BCEM
Main Effects	B	.0001	.0001	.0001	.0001	.0001	.0001	.0001
	T	.0001	.0001	.0001	.0001	.0001	.0001	.0001
	D	.0001	.0001	.0001	.0001	.0001	.0001	.0261
Interaction Effects	BT	.0095	.0077	.0495	.0001	.0001	.0001	.0009
	BD	.0001	.0001	.0001	.0001	.0001	.0001	N.S.
	TD	.0001	.0001	.0001	.0001	.0003	.0001	.0007
	BTD	N.S.	N.S.	N.S.	.0003	.0001	.0001	N.S.

a. Factors

B = Buffering Strategy
 T = Type of Supply Uncertainty
 D = Degree of Supply Uncertainty
 BT = Interaction Between B and T
 BD = Interaction Between B and D
 TD = Interaction Between T and D

b. Performance Measures

HOLC = Inventory Carrying Cost
 INVC = Total Setup and Carrying Cost
 TOC = Total Cost
 BO = Total Number of Units Short
 STK = Total Number of Stockouts
 SLVL = Service Level
 BCEM = Buffering Cost Effectiveness

Note:

1. The first six performance measures are in terms of the planning horizon (52 periods). BCEM is for each extra one hundred thousand dollars inventory invested.
2. This description of both the factors and the performance measures holds for all subsequent tables.

the assumption of normality and equality of variances in most cases. Therefore, using Tukey's test is justified.

Whenever the F-test lead to the conclusion that the factor level means differed significantly, Tukey's test was utilized to examine how the different factor levels compare with one another in terms of the system performance measurement. The results of this test are reported in Tables B.3 through B.5 in Appendix B. A summary is reported in Tables 4.2 through 4.4.

In general, Table 4.1 indicates that the main effects due to all factors are significant with respect to each of the seven performance measures. All the two-way interaction effects are also significant with respect to each of the seven performance measures with one exception. The interaction between factors "buffering strategy" and "degree of supply uncertainty" has no significant effect at .05 level on the "buffering cost effectiveness" criterion. For only three of the seven performance criteria was the three-way interaction found to be significant ($P < .001$)

The findings of ANOVA presented in Tables A.1 through A.7 and in Table 4.1 are used in the next part to test each of the null hypotheses presented in Chapter III. The results of the Tukey's test are utilized to support the analysis concerning the significance between different level means for each factor.

Null Hypothesis No. 1. It was hypothesized that different buffering strategies have no significant effect on the system performance.

The results of the ANOVA reported in Table 4.1 indicate that the main effect of the factor "buffering strategy" is significant at the .01 level for all performance criteria. Therefore this hypothesis is

rejected. This implies that the system performance might be significantly different for any of the seven performance measures based on the particular buffering strategy(s) adopted. This conclusion is consistent with both the Whybark and Williams (58), and the Liaw (32) results. Although the first study was considering only a single item, it implies that significant differences exist in terms of service level when using safety stock rather than safety lead time or vice-versa. Liaw also reported that a significant main effect was found for "safety stock policy" factor in terms of the number of stockouts and number of outages. It should be noted that Liaw did not consider providing safety lead time as a way of buffering the system against uncertainty. Therefore his conclusions must be taken with caution when comparing results.

This finding that different buffering strategies have different impacts upon the performance of the system is not surprising. New (41), without any empirical evidence, indicated that each strategy is likely to have its own distinct operating characteristic. For instance, a safety time policy will cause the projected stock to vary widely from period to period while a fixed buffer policy requires the buffer quantity to be held all the time. Therefore they were expected to perform differently in terms of inventory cost and service level, under different production environments.

In order to explore how the multilevel buffering strategies differ in terms of the effects on system performance, Tukey's test results are used. Table 4.2 indicate that (a) all strategies performed significantly differently in terms of the first two response variables: holding cost and inventory cost, (b) both strategy 1 (SS/SS) and strategy 6 (SS/0) performed almost the same in terms of the total cost variable

TABLE 4.2
A SUMMARY OF TUKEY'S MULTIPLE COMPARISON TEST
FOR BUFFERING STRATEGIES*

$$\alpha = .05$$

SUBSET	Performance Measure						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
A	3	3	3	5	5	3,4	6
B	4	4	4	6	6	2,1	1,2
C	2	2	2	1,2	1,2	6	2,4,3
D	1	1	1,6	4,3	3,4	5	
E	6	6	5				
F	5	5					

*1 = (SS/SS), 2 = (SS/SLT), 3 = (SLT/SLT), 4 = (SLT/SS), 5 = (0/0),
6 = (SS/0)

measure. When considering the number of shortages and service level, the table shows that (a) both strategies 5(0/0) and 6(SS/0) performed significantly different from any other strategy, (b) both strategies 1(SS/SS) and 6(SS/0) performed almost the same. The table shows also that the difference between the last three response variables generated from strategies 3(SLT/SLT) and 4(SLT/SS) is not significant. As for buffering cost effectiveness measure, strategy 6(SS/0) is performing significantly different from any other buffering strategy while no significant

difference existed among strategies 4(SLT/SS), 3(SLT/SLT), and 2(SS/SLT) or among strategies 2(SS/SLT) and 1(SS/SS).

In summary, the most pronounced difference across all performance measures is between strategy 3(SLT/SLT) and strategy 5(0/0) with one exception. In terms of buffering cost effectiveness, the most significant difference is between strategy 6(SS/0) and strategy 3(SLT/SLT).

Null Hypothesis No. 2. It was hypothesized that different supply uncertainty types have no significant effect on the system performance.

The ANOVA data presented in Table 4.1 suggest that the main effect of the factor "type of supply uncertainty" is significant at the .01 level with respect to all performance criteria. Therefore this hypothesis is rejected.

Tukey's test was conducted to understand how the four types of supply uncertainty differed in terms of their effect on all performance measures. Table 4.3 summarizes the results.

Across all cost performance measures, Table 4.3 indicates that the difference between the effect of supply uncertainty type 4(Q/T) and any other supply uncertainty type is significant, while the difference is almost negligible between the effects of type 2(Q/Q) and type 3(T/Q) in terms of holding cost only. On the other hand, all differences are significant among all uncertainty types in terms of the number of shortages, number of stockouts and the service level. Type 3(T/Q) is the only type to differ significantly in terms of buffering cost effectiveness measure.

In summary, the most noticeable difference cost criteria exists between types 4(Q/T) and 3(T/Q) while the next most is between 4(Q/T) and 2(Q/Q). Another interesting finding is that the difference

TABLE 4.3

A SUMMARY OF TUKEY'S MULTIPLE COMPARISON TEST
FOR TYPE OF SUPPLY UNCERTAINTY*

$$\alpha = .05$$

SUBSET	Performance Measure						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
A	4	4	1	1	1	2	3
B	1	1,2	3	3	3	4	1,4,2
C	2,3	3	4	4	4	3	
D			2	2	2	1	

*1 = (T/T), 2 = (Q/Q), 3 = (T/Q), 4 = (Q/T)

between types 2(Q/Q) and 1(T/T) is insignificant in terms of inventory cost criterion while the difference between the same two uncertainty types, 2(Q/Q) and 1(T/T), is reported to be the most significant according to service level criterion. This leads to the conclusion that the effect of different uncertainty types on the performance of the system depends on the criteria used to judge the performance of the system.

Null Hypothesis No. 3. It was hypothesized that different supply uncertainty levels have no significant effect on the system performance.

Table 4.1 indicates that the main effect of the factor "degree of supply uncertainty" is significant at the .01 level with respect to performance measures one through six and significant at .05 level with

respect to the last criterion "buffering cost effectiveness." Therefore, this hypothesis is rejected.

This conclusion is, to some extent, congruent with the results reported by most previous empirical buffering strategies studies including Whybark and Williams (58) and Liaw (32). Whybark and Williams concluded that both the coefficient of variation and the level of supply uncertainty have a significant effect on the service level at the .05 level for each uncertainty category. Liaw reported also a significant effect for the inventory risk on the number of stockouts and number of outages.

Tukey's test was conducted to explore how the four multilevel combinations of supply uncertainty degree differed in terms of the effect on all performance measures. Table 4.4 summarized these results.

The table reveals that the difference between degree 2(L/L) and degree 1(H/H) represents the largest difference across all performance measures. This result was expected because of the distinguished behavior of the number of shortages, service level, and shortage cost under each of these uncertainty conditions. A system operating under a high degree of uncertainty at all levels should incur a higher number of shortages, a lower service level and a higher shortage cost than a system operating under a low degree of uncertainty.

Null Hypothesis No. 4. It was hypothesized that different types of supply uncertainty have no effect on the performance of the buffering strategies.

Table 4.1 shows that the interaction effect of these two factors is significant at .05 level for all performance measures. Therefore, this hypothesis is rejected.

TABLE 4.4
A SUMMARY OF TUKEY'S MULTIPLE COMPARISON TEST
FOR DEGREE OF SUPPLY UNCERTAINTY*

$$\alpha = .05$$

SUBSET	Performance Measure						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
A	1	1	1	1	1	2	2,4,3
B	4,3	4	4	3	3	4	4,3,1
C	2	3	3	4	4	3	
D		2	2	2	2	1	

*1 = (H/H), 2 = (L/L), 3 = (H/L), 4 = (L/H)

Null Hypothesis No. 5. It was hypothesized that different degree of supply uncertainty has no effect on the performance of different buffering strategies.

Table 4.1 indicates that the interaction effect of these two factors is significant at .01 level for all performance measures with only one exception. The interaction effect is negligible with respect to the buffering cost effectiveness measure. Therefore, this hypothesis is rejected.

This conclusion seems to reinforce Whybark and Williams' (58) results with respect to choosing between safety stock and safety lead time.

Null Hypothesis No. 6.

In this section, a comparison of the relative performance of all buffering strategies is presented and discussed. The results of this discussion are then used to test null hypothesis number six concerning the existence of any preference pattern among all buffering strategies. In order to test that, all buffering strategies were ranked in terms of the different performance criteria. These ranks were presented in Table 4.5. This table, in conjunction with Tukey's test results in Table 4.2, is used to explore any significant rank difference among all buffering strategies. It should be noted at this point that these comparisons are in terms of the overall performance of the buffering strategies without discussing any potential effects of both uncertainty types and level on the performance of a particular strategy. This analysis will be performed in a later section.

Examination of Tables 4.2 and 4.5 reveals the following points:

- (1) According to all cost criteria, buffering strategy 5(0/0) performed better than any other strategy. Apparently this is due to the minimal inventory cost incurred because no extra inventory is carried at any level according to this strategy. Because the total cost criterion includes the total shortage cost, which is expected to be relatively high in this case, this performance of strategy 5 seems to indicate that this high shortage cost is offset with a very low inventory investment. This might also indicate that the cost structure applied in this study involves a relatively low shortage cost compared to the carrying cost. Further investigation of the effect of different cost structures seems required.

TABLE 4.5
 BUFFERING STRATEGIES RANKED IN TERMS OF
 DIFFERENT PERFORMANCE MEASURES
 (Ranking is based on the overall mean values)

BUFFERING STRATEGY	Performance Measures						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
1 SS/SS	3	3	3	4	4	4	2
2 SS/SLT	4	4	4	3	3	3	3
3 SLT/SLT	6	6	6	1	2	1	5
4 SLT/SS	5	5	5	2	1	2	4
5 0/0	1	1	1	6	6	6	NA
6 SS/0	2	2	2	5	5	5	1

(2) A close examination of the meaning of all ranks reported in Table 4.5, in light of the results reported in Table 4.2, might reverse the previous conclusion. Table 4.2 shows that the differences between strategies 6(SS/0) and 1(SS/SS) is insignificant regarding total cost criterion. Therefore, if strategy 5 (no buffering) is not considered, both strategies 6(SS/0) and 1(SS/SS) would be ranked first for the total cost criterion, and with significant differences from strategies 2(SS/SLT), 3(SLT/SLT), and 4 (SLT/SS).

(3) The relative lower ranks for strategies 2(SS/SLT), 3(SLT/SLT) and 4(SLT/SS) seems to indicate that if safety lead time is used at either level (higher and/or lower), inventory cost tends to be relatively high.

(4) As expected, buffering strategy 5(0/0) showed the poorest performance results in terms of the number of shortages, number of stockouts and service level. Table 4.2 supports this by indicating that the difference between 5(0/0) and any other strategy is significant.

(5) Strategy 3(SLT/SLT) provides the best protection against supply uncertainty. This strategy was at the top of the list for both number of shortages and service level. However, the difference between this strategy and strategy 4(SLT/SS) is reported to be insignificant. This might imply that using safety lead time for upper level items (end and intermediate items) will yield a good service level regardless of the strategy at the lower level (raw materials) might be. Again, if strategy 5 (no buffering) is not considered, both strategies 6(SS/0) and 1(SS/SS) were the worst in terms of number of shortages and service level criteria. This indicates that the rank for both strategy 6(SS/0) and strategy 1(SS/SS) would be reversed if the performance criterion used is service level rather than inventory cost. At this point, it is also concluded that providing safety stock at all levels or for finished and intermediate items only is more likely to yield the lowest inventory cost but the poorest service level. This conclusion challenges, to some extent, depending on safety stock as the only buffering technique in the multilevel production environment without considering safety lead time as an alternative means to provide protection against supply uncertainty.

(6) From an economic point of view, it seems that strategy 6(SS/0) is the best. This policy out performed all other strategies when considering the buffering cost effectiveness measure. Moreover, strategy 1(SS/SS) ranked the second best with a significant difference from strategy 3(SLT/SLT). Strategy 3, which was the best in terms of the amount of protection provided, is among the worst performance based on the buffering cost effectiveness. In general, Table 4.2 reveals that providing safety lead time at any level (strategies 2, 3, 4) has no economic justification, i.e., the increase in the service level does not justify the extra inventory cost under any of these policies.

(7) Strategy 2(SS/SLT) which was recommended by New (41) never proved to be the best, or even the next best, for any of the response variables.

This analysis shows that some strategies are preferred in terms of all cost criteria while they are undesirable in terms of the number of shortages and service level response variables. Both strategies 6(SS/0) and 5(0/0) are examples of this case. Moreover, the same strategy 6(SS/0) is highly desirable with respect to the buffering cost effectiveness measures. These results seem to lead to rejection of hypothesis number six.

The Effect of Type and Degree of Uncertainty on Selecting a Buffering Strategy.

The analysis up to this point has demonstrated that a buffering strategy may result in different costs and service levels with different supply types and levels. Consequently, one strategy might be preferred under particular uncertainty conditions while the same strategy is undesirable under some other circumstances. This section investigates, in detail, how supply uncertainty types and levels might effect the

performance of a given buffering strategy with respect to some key performance measures. These include inventory cost, service level and buffering cost effectiveness.

Although some conclusions in this part are not statistically significant, this investigation may indicate general behavior of particular strategy under specific uncertainty conditions. Through the plots of the means of these response variables generated for each strategy under all combinations of uncertainty types and levels, conclusions regarding the relationships between a buffering strategy and uncertainty conditions might be drawn. Figures C.1 through C.12 present the data reported in Tables C.1 through C.4 for the three performance measures.

Inventory Cost

With respect to inventory cost, Figures C.1 through C.4 show the following:

- (1) Buffering strategies 5(0/0) and 6(SS/0) result in the lowest inventory cost. Since strategy 5(0/0) is a "no buffering" policy, strategy 6(SS/0) might be considered the best among all buffering strategies.
- (2) If the uncertainty involved at each inventory level is sufficiently low (L/L), the range of the total inventory costs among all the buffering strategies is lower than with the other uncertainty situations.
- (3) If the production-inventory system is facing timing uncertainty at both levels (T/T), the range of the total inventory costs between strategies 1(SS/SS) and 6(SS/0) tends to be lower than with the quantity uncertainty at both levels case (Q/Q). This is true in three of the four uncertainty level combinations.
- (4) Apparently providing safety lead time at both levels (SLT/SLT) is the worst strategy under all uncertainty conditions. This implies that

it is performing poorly when the system is operating under timing uncertainty at both level (T/T) as well.

(5) Providing safety lead times for upper level items and safety stock for lower level items (SLT/SS) did not perform among the best under the mixed uncertainty case (T/Q). To the contrary, this strategy performs as poorly as the poorest strategy (strategy 3) when a high uncertainty level exists at both levels (H/H) or at the higher level only (H/L).

Service Level

In terms of the service level, Figures C.5 through C.8 show the following:

(1) Buffering strategies 3(SLT/SLT) and 4(SLT/SS) are always among the top performing strategies under all uncertainty types and levels. As expected, strategy 5 (no buffering) consistently showed the poorest performance results.

(2) No noticeable difference is demonstrated among all buffering strategies (except 5) if the system is operating under uncertainty levels 2(L/L) or 3(H/L).

(3) Providing safety stock for finished product and intermediate items only (SS/0) seems undesirable in general especially if the system is facing a high uncertainty at both levels (H/H) or at lower level only (L/H). Moreover, this strategy should be avoided completely if finished and intermediate items are encountering timing uncertainty and high quantity uncertainty exists at the raw material level items.

(4) The insignificant difference among strategies 1 through 4 in most cases seems to challenge Whybark and Williams' (58) logic, SLT for timing uncertainty and SS for quantity uncertainty, when considering buffering a multilevel inventory system if service level is the criterion.

Buffering Cost Effectiveness

With respect to buffering cost effectiveness measure, Figure C.9 through C.12 show the following:

- (1) Providing safety stocks for finished and intermediate items only, strategy 6(SS/0), outperformed all other strategies under most uncertainty conditions.
- (2) Strategy 6(SS/0) had outstanding performance in two cases as shown in Figures C.10 and C.12. The first case is when both finished and intermediate items encounter low timing uncertainty while raw material items are expecting low quantity uncertainty (LT/LQ). The second case is when upper level items, finished and intermediate, are expecting a low timing uncertainty but low level items, raw materials, are expecting a high quantity uncertainty (LT/HQ).
- (3) Surprisingly, neither strategies 2(SS/SLT), 3(SLT/SLT) or 4(SLT/SS) performed well when the system is operating under timing uncertainty at both levels (T/T). They are almost the poorest strategies under this uncertainty condition. This result strongly suggests not to use safety lead time at any level as a part of the buffering strategy in the multi-level buffering case. Once more, this result seems not to confirm the Whybark and Williams' (58) conclusion that using safety lead time is preferred when buffering against timing uncertainty.

CHAPTER V

SUMMARY AND CONCLUSIONS

Objective of the Study

The main objective of this research was to provide some insights into the behavior of a hypothetical multistage multiproduct production-inventory system using different buffering strategies to face different supply uncertainty conditions. Therefore, investigation of the relative effect of different joint (multilevel) buffering strategies on the performance of the system was possible. Moreover, an attempt was made to establish some guidelines for choosing among different buffering strategies when buffering the system against different combinations of supply uncertainty types and levels. Several performance criteria, including inventory cost, service level and buffering cost effectiveness were used to evaluate system performance.

Tests of Hypotheses

Three null hypotheses concerning the main effects of buffering strategy, degree of supply uncertainty and type of supply uncertainty on system performance were presented. The effect of the latter two factors on buffering strategies was also hypothesized in null hypotheses 4 and 5. Finally, null hypothesis 6 was presented to test the existence of any "preference" pattern among different buffering strategies.

The analysis of variance (ANOVA) procedure was used to test the first five null hypotheses concerning the main and interaction effects of the three factors on each of the response variables. Whenever the F-test lead to the conclusion that the factor level means different significantly, Tukey's test was utilized to examine how the different factor levels compare with one another in terms of the system performance

measurements. All buffering strategies were ranked according to the overall means of the different performance criteria. These ranks, in conjunction with Tukey's test results were used to test null hypothesis number six. The results of the statistical analysis testing these hypotheses are summarized below.

1. The system performance is affected by the choice of buffering strategy with respect to all seven performance measures employed in this research.
2. The system performance is affected by degree of supply uncertainty with respect to all seven performance measures employed in this research.
3. The system performance is affected by type of supply uncertainty with respect to all seven performance measures employed in this research.
4. Type of supply uncertainty is a significant decision variable regarding the selection of an appropriate buffering strategy according to all performance measures.
5. Degree of supply uncertainty is a significant decision variable regarding the selection of an appropriate buffering strategy according to six of the seven performance measures. The effect of supply uncertainty types on buffering strategy with respect to buffering cost effectiveness measure is not significant.
6. Some strategies are preferred in terms of all cost criteria while they are undesirable in terms of the number of shortages, service level, and buffering cost effectiveness. The opposite was also true for some other strategies, i.e., the "preference" depends on the criteria used to judge the performance of the system.

Summary and Conclusions

The results of the present study show that performance of the production system is significantly influenced by the "buffering strategy" factor. This implies that the system might perform significantly differently, in terms of any of the used seven performance measures, when adapting a particular buffering strategy. Although the relative impact of the strategies is dependent on the performance measure considered, this conclusion seems to be consistent with both the Whybark and Williams (58), and the Liaw (32).

The effect of different uncertainty types on the performance of the system, for this study, is also noticeable for most performance measures. For instance, a system operating under quantity uncertainty at the upper level (finished and intermediate items) and timing uncertainty at the lower level (raw material items) incurs a relatively higher cost than a system operating under the reversed circumstances, i.e., quantity at the lower level and timing at the higher level (T/Q). Another interesting finding is that the difference between conditions of quantity uncertainty at all levels (Q/Q) and timing uncertainty at all levels (T/T) is insignificant in terms of inventory cost, while the difference between the same two uncertainty types, 2(Q/Q) and 1(T/T), is reported to be the most significant according to service level criterion.

The study also shows that degree of supply uncertainty has a significant impact on system performance. A system operating under a high degree of uncertainty at all levels is likely to incur a higher number of shortages, a lower service level and a higher shortage cost than a system operating under a low degree of uncertainty. Moreover, it was

reported that having a higher degree of uncertainty at the upper level (finished and intermediate items) will cause a poor system performance regardless of the degree of uncertainty at the lower level (raw material items) might be. This latter observation can be used to explain the relative importance of the finished and intermediate items.

This research provides empirical evidence that both supply uncertainty type and level are significant decision variables regarding the selection of an appropriate buffering strategy. Interactions between buffering strategy and either type of supply uncertainty or degree of supply uncertainty were found to be significant in most cases. This result indicates that an identification of the uncertainty conditions encountered by the system at each level is a recommended step to make the best of buffering strategies in a multistage, multiproduct production-inventory environment.

With respect to the relative impact of different buffering strategies, the study indicates that it depends on the criteria used to judge the performance of the system. Some strategies were found to be preferred in terms of the cost criteria while they are undesirable in terms of the number of shortages and service level. For instance, providing safety stock at all inventory levels (strategy 1) or for finished and intermediate items only (strategy 6) are more likely to yield the lowest inventory cost but the poorest service level. Another example is strategy 3(SLT/SLT). Providing safety lead time at both levels (strategy 3) yields the best service level but the lowest buffering cost effectiveness in all cases. Thus, the benefits of this strategy are questionable due to its relatively high cost. This result seems to suggest not to use safety lead time at all levels as a buffering strategy. However, a

relatively high unit shortage cost to holding cost may alter this conclusion. More research is warranted in this area.

The investigation of the effect of different uncertainty conditions on the performance of different buffering strategies was also conducted in this research to conclude some guidelines which might help the practitioner in selecting the appropriate buffering strategy. These guidelines are summarized in this section according to three selected performance measures. These are inventory cost, service level and buffering cost effectiveness.

According to inventory cost, the investigation indicates that if the uncertainty involved at each inventory level is sufficiently low (L/L), the range of the total inventory cost among all the buffering strategies is lower than with the other uncertainty situations. In light of this observation, it is recommended to MRP users to assess the degree of uncertainty existed at all stages in the system before searching for the "most appropriate" buffering strategy. Under low uncertainty, there always exists a set of "accepted" buffering strategies, among which one can be selected. On the other hand, when the degree of uncertainty at both levels increases, the importance of making the right choice among buffering strategies increases. It is observed also that providing safety lead time at both levels (SLT/SLT) represents the poorest strategy under all uncertainty conditions in terms of inventory cost. Overall, providing safety lead time does not prove to be the best method to protect the system against timing uncertainty. Consistently, strategy 6(SS/0) outperforms all other strategies for all cost criteria.

When unit shortage cost is relatively high, MRP users might be interested in using service level as the performance measure. Under

such circumstances, using safety lead time at both levels (SLT/SLT) or at upper level only (SLT/SS) are the most recommended strategies. They are always among the top performing strategies under all uncertainty types and levels. Under this case, users must also avoid using strategy 6(SS/0), especially if the system is facing a high uncertainty at both levels (H/H). Using this policy under this circumstance will cause a higher number of shortages and a lower service level. According to the overall performance measure (buffering cost effectiveness) strategy 6(SS/0) seems appropriate. This strategy out performs all other strategies in most cases.

In conclusion, the use of strategy 6(SS/0) is recommended for a lower inventory cost and better buffering cost effectiveness while providing lead times at all levels (SLT/SLT) is recommended for lower shortages and a higher service level.

Toward the end of this research, it is important to mention that all concluded findings during the course of this research should be viewed with a certain amount of caution. These findings are based on the characteristics of the specific simulated system, including the product and cost structures, demand patterns, production system structure, and other specifications resulting from the stated assumptions. To generalize these results, to any extent, requires further investigation along these lines.

Directions for Future Research

Several assumptions have been made to keep the size of this study reasonable. Simply by relaxing any of these assumptions, new avenues of research will be available.

Additional research is warranted to determine why some buffering strategies are superior under a particular uncertainty environment. A close examination of the data, on a case-by-case basis, may be helpful in understanding why a particular strategy affects the system in a specific way under each uncertainty conditions. Many other areas for additional research remain. An obvious extension of this research would be to examine the impact of altering both system structure (more than three stages) and product structure (degree of commonality) on the reported results. The problem will be more complicated if the lead times are different among levels, especially when a parent item requires some component items with considerably different lead time lengths. The effect of different cost structures (unit shortage cost to unit holding cost) on the relative performance of each buffering strategy is another area open to further investigation. Examining the interaction between buffering decisions and various lot-sizing techniques and the effect of demand uncertainty, in addition to supply uncertainty, would be most interesting and would provide a valuable contribution to the body of research in this area.

APPENDIX A
THE RESULTS OF ANALYSIS OF VARIANCE

TABLE A.1

ANALYSIS OF VARIANCE-FIXED EFFECT MODEL

Source of Variation: Buffering Strategy (B)

No.	Performance Measure	Observed F Statistic	PR > F
1	Inventory Carrying Cost	195.38**	.0001
2	Total Setup and Carrying Costs	195.02**	.0001
3	Total Cost	167.04**	.0001
4	Total Number of Units Short	1656.33**	.0001
5	Total Number of Stockouts	748.24**	.0001
6	Service Level	1672.27**	.0001
7	Buffering Cost Effectiveness	19.34**	.0001

$F_{.95} (5, 384) = 2.21$, $F_{.99} (5, 384) = 3.02$

TABLE A.2

ANALYSIS OF VARIANCE-FIXED EFFECT MODEL

Source of Variation: Type of Supply Uncertainty (T)

No.	Performance Measure	Observed F Statistic	PR > F
1	Inventory Carrying Cost	60.58**	.0001
2	Total Setup and Carrying Costs	76.50**	.0001
3	Total Cost	61.22**	.0001
4	Total Number of Units Short	495.53**	.0001
5	Total Number of Stockouts	78.27**	.0001
6	Service Level	509.42**	.0001
7	Buffering Cost Effectiveness	9.39**	.0001

$$F_{.95} (3, 384) = 2.60, F_{.99} (3, 384) = 3.78$$

TABLE A.3

ANALYSIS OF VARIANCE-FIXED EFFECT MODEL

Source of Variation: Degree of Supply Uncertainty (D)

No.	Performance Measure	Observed F Statistic	PR > F
1	Inventory Carrying Cost	99.00**	.0001
2	Total Setup and Carrying Costs	85.53**	.0001
3	Total Cost	81.83**	.0001
4	Total Number of Units Short	440.44**	.0001
5	Total Number of Stockouts	83.96**	.0001
6	Service Level	439.10**	.0001
7	Buffering Cost Effectiveness	3.12*	.0261

$F_{.95} (3, 384) = 2.60$, $F_{.99} (3, 384) = 3.78$

TABLE A.4

ANALYSIS OF VARIANCE-FIXED EFFECT MODEL

Source of Variation: Interaction Between B and T

No.	Performance Measure	Observed F Statistic	PR > F
1	Inventory Carrying Cost	2.10**	.0095
2	Total Setup and Carrying Costs	2.15**	.0077
3	Total Cost	1.70*	.0485
4	Total Number of Units Short	43.19**	.0001
5	Total Number of Stockouts	9.75**	.0001
6	Service Level	45.36**	.0001
7	Buffering Cost Effectiveness	2.87**	.0009

$$F_{.95} (15, 384) = 1.67, F_{.99} (15, 384) = 2.04$$

TABLE A.5

ANALYSIS OF VARIANCE-FIXED EFFECT MODEL

Source of Variation: Interaction Between B and D

No.	Performance Measure	Observed F Statistic	PR > F
1	Inventory Carrying Cost	11.44**	.0001
2	Total Setup and Carrying Costs	11.30**	.0001
3	Total Cost	11.04**	.0001
4	Total Number of Units Short	125.93**	.0001
5	Total Number of Stockouts	29.39**	.0001
6	Service Level	125.64**	.0001
7	Buffering Cost Effectiveness	1.34	.1952

$$F_{.95} (15, 384) = 1.67, F_{.99} (15, 384) = 2.04$$

TABLE A.6

ANALYSIS OF VARIANCE-FIXED EFFECT MODEL

Source of Variation: Interaction Between T and D

No.	Performance Measure	Observed F Statistic	PR > F
1	Inventory Carrying Cost	11.08**	.0001
2	Total Setup and Carrying Costs	11.97**	.0001
3	Total Cost	10.85**	.0001
4	Total Number of Units Short	12.74**	.0001
5	Total Number of Stockouts	3.64**	.0003
6	Service Level	12.81**	.0001
7	Buffering Cost Effectiveness	3.36**	.0007

$F_{.95}(9, 384) = 1.88$, $F_{.99}(9, 384) = 2.41$

TABLE A.7

ANALYSIS OF VARIANCE-FIXED EFFECT MODEL

Source of Variation: Interaction Between B, T and D

No.	Performance Measure	Observed F Statistic	PR > F
1	Inventory Carrying Cost	.87	.7165
2	Total Setup and Carrying Costs	.86	.7256
3	Total Cost	.85	.7473
4	Total Number of Units Short	2.00	.0003
5	Total Number of Stockouts	3.25	.0001
6	Service Level	2.23	.0001
7	Buffering Cost Effectiveness	1.05	.3990

$$F_{.95} (45, 384) = 1.35, F_{.99} (45, 384) = 1.59$$

APPENDIX B
THE RESULTS OF TUKEY'S
MULTIPLE COMPARISON TEST

TABLE B.1
D STATISTIC FOR THE MODIFIED VERSION OF
KOLMOGOROV-SMIRNOV TEST OF NORMALITY,
FOR ALL PERFORMANCE MEASURES

PERFORMANCE	D-STATISTIC	PROB>D
HOLC	0.17037	<0.01
INVC	0.151875	<0.01
TOC	0.156375	<0.01
BO	.216795	<0.01
STK	0.22551	<0.01
SLVL	0.218704	<0.01
RRHTH	0.264667	<0.01

Conclusion: Normality assumption is satisfied for all performance measures.

TABLE B.2
 THE HARTLEY'S TEST STATISTIC H FOR
 ALL PERFORMANCE MEASURES AND
 FACTOR LEVELS

$$\alpha = .01$$

Performance Measure	Among B Levels ⁽¹⁾	Among T Levels ⁽²⁾	Among D Levels ⁽²⁾
HOLC	17.380	3.397	9.808
INVC	14.157	3.679	9.078
TOC	15.428	3.956	8.225
BO	37.937	2.532	8.146
STK	43.784	1.370	3.703
SLVL	38.412	2.565	7.810
BCEM	134.623 ⁽³⁾	29.592	23.500

(1) $H_{(.99, r = 6, n = 5)} = 69$

(2) $H_{(.99, r = 4, n = 5)} = 49$

(3) $H_{(.99, r = 5, n = 5)} = 59$

Decision Rule:

If $H \leq H_{(1-\alpha; r, n)}$, Conclude $C_1 : \sigma_1^2 = \sigma_2^2 = \sigma_3^2 = \dots = \sigma_r^2$

If $H > H_{(1-\alpha; r, n)}$, Conclude $C_2 : \text{not all } \sigma_i^2 \text{ are equal.}$

Conclusion:

The equality of variances assumption is fulfilled for all measures among each factor levels with one exception. The assumption is not fulfilled for BCEM among factor B levels.

TABLE B.3
 TUKEY'S MULTIPLE COMPARISON TEST
 FOR BUFFERING STRATEGY

$$\alpha = .05$$

SUBSET	GROUPS
<u>Performance Measure: HOLC</u>	
A	3(SLT/SLT)
B	4(SLT/SS)
C	2(SS/SLT)
D	1(SS/SS)
E	6(SS/0)
F	5(0/0)
<u>Performance Measure: INVC</u>	
A	3(SLT/SLT)
B	4(SLT/SS)
C	2(SS/SLT)
D	1(SS/SS)
E	6(SS/0)
F	5(0/0)
<u>Performance Measure: TOC</u>	
A	3(SLT/SLT)
B	4(SLT/SS)
C	2(SS/SLT)
D	1(SS/SS), 6(SS/0)
E	5(0/0)

TABLE B.3 (Continued)

<u>Performance Measure: BO</u>	
A	5(0/0)
B	6(SS/0)
C	1(SS/SS), 2(SS/SLT)
D	4(SLT/SS), 3(SLT/SLT)
<u>Performance Measure: STK</u>	
A	5(0/0)
B	6(SS/0)
C	1(SS/SS), 2(SS/SLT)
D	3(SLT/SLT), 4(SLT/SS)
<u>Performance Measure: SLVL</u>	
A	3(SLT/SLT), 4(SLT/SS)
B	2(SS/SLT), 1(SS/SS)
C	6(SS/0)
D	5(0/0)
<u>Performance Measure: BCEM</u>	
A	6(SS/0)
B	1(SS/SS), 2(SS/SLT)
C	2(SS/SLT), 4(SLT/SLT), 3(SLT/SLT)

TABLE B.4
 TUKEY'S MULTIPLE COMPARISON TEST
 FOR TYPE OF SUPPLY UNCERTAINTY

$$\alpha = .05$$

SUBSET	GROUPS
<u>Performance Measure: HOLC</u>	
A	4(Q/T)
B	1(T/T)
C	2(Q/Q), 3(T/Q)
<u>Performance Measure: INVC</u>	
A	4(Q/T)
B	1(T/T), 2(Q/Q)
C	3(T/Q)
<u>Performance Measure: TOC</u>	
A	1(T/T)
B	3(T/Q)
C	4(Q/T)
D	2(Q/Q)
<u>Performance Measure: BO</u>	
A	1(T/T)
B	3(T/Q)
C	4(Q/T)
D	2(Q/Q)

Table B.4 (Continued)

<u>Performance Measure: STK</u>	
A	1(T/T)
B	3(T/Q)
C	4(Q/T)
D	5(Q/Q)
<u>Performance Measure: SLVL</u>	
A	2(Q/Q)
B	4(Q/T)
C	3(T/Q)
D	1(T/T)
<u>Performance Measure: BCEM</u>	
A	3(T/Q)
B	1(T/T), 4(Q/T), 2(Q/Q)

TABLE B.5
 TUKEY'S MULTIPLE COMPARISON TEST
 FOR DEGREE OF SUPPLY UNCERTAINTY

$$\alpha = .05$$

SUBSET	GROUPS
<u>Performance Measure: HOLC</u>	
A	1 (H/H)
B	4 (L/H), 3 (H/L)
C	2 (L/L)
<u>Performance Measure: INVC</u>	
A	1 (H/H)
B	4 (L/H)
C	3 (H/L)
D	2 (L/L)
<u>Performance Measure: TOC</u>	
A	1 (H/H)
B	4 (L/H)
C	3 (H/L)
D	2 (L/L)
<u>Performance Measure: BO</u>	
A	1 (H/H)
B	3 (H/L)
C	4 (L/H)
D	2 (L/L)

TABLE B.5 (Continued)

<u>Performance Measure: STK</u>	
A	1(H/H)
B	3(H/L)
C	4(L/H)
D	2(L/L)
<u>Performance Measure: SLVL</u>	
A	2(L/L)
B	4(L/H)
C	3(H/L)
D	1(H/H)
<u>Performance Measure: BCEM</u>	
A	2(L/L), 4(L/H), 3(H/L)
B	4(L/H), 3(H/L), 1(H/H)

TABLE B.4
 MEAN VALUES OF ALL PERFORMANCE MEASURES FOR
 DIFFERENT BUFFERING STRATEGY LEVELS

BUFFERING STRATEGY	Performance Measure						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
1 (SS/SS)	4399011.	5696064.	5716908.	2651	21	.9492	5.003C
2 (SS/SLT)	5774867.	7058400.	7118643.	2384	18	.9542	2.8997
3 (SLT/SLT)	7949158.	9218915.	9262057.	1819	12	.9650	1.7641
4 (SLT/SS)	6441580.	7728412.	7833235.	1876	12	.9639	2.5527
5 (O/O)	2992965.	4267145.	4414256.	9215	78	.8216	NA
6 (SS/O)	3823996.	5106880.	5177692.	3641	32	.9296	8.5542

TABLE B.5
 MEAN VALUES OF ALL PERFORMANCE MEASURES FOR
 DIFFERENT TYPES OF SUPPLY UNCERTAINTY

TYPE OF SUPPLY UNCERTAINTY	Performance Measure						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
1 (T/T)	5502899.	653391.	6661081.	5075	36	.9014	3.8278
2 (Q/Q)	4645480.	6152078.	6229350.	2125	20	.9593	2.6560
3 (T/Q)	4487193.	5576480.	5671005.	4066	31	.9218	6.6013
4 (Q/T)	6287336.	7778196.	7786982.	3126	27	.9399	3.5341

TABLE B.6
 MEAN VALUES OF ALL PERFORMANCE MEASURES FOR
 DIFFERENT DEGREES OF SUPPLY UNCERTAINTY LEVELS

DEGREE OF SUPPLY UNCERTAINTY	Performance Measure						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
1 (H/H)	6474212.	7651837.	7760093.	4958	36	.9045	2.9745
2 (L/L)	3886796.	5253766.	5267746.	2078	20	.9601	5.1956
3 (H/L)	5120979.	6330905.	6440000.	3888	32	.9250	3.7739
4 (L/H)	5230729.	6793945.	6880584.	3467	29	.9328	4.6751

TABLE B.7

TYPE OF SUPPLY UNCERTAINTY LEVELS RANKED IN TERMS OF
DIFFERENT PERFORMANCE MEASURES

TYPE OF SUPPLY UNCERTAINTY	Performance Measures						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
1 T/T	3	3	3	4	4	4	2
2 Q/Q	2	2	2	1	1	1	4
3 T/Q	1	1	1	3	3	3	1
4 Q/T	4	4	4	2	2	2	3

TABLE B.8

DEGREE OF SUPPLY UNCERTAINTY LEVELS RANKED IN TERMS OF
DIFFERENT PERFORMANCE MEASURES

DEGREE OF SUPPLY UNCERTAINTY	Performance Measures						
	HOLC	INVC	TOC	BO	STK	SLVL	BCEM
1 H/H	4	4	4	4	4	4	4
2 L/L	1	1	1	1	1	1	1
3 H/L	2	2	2	3	3	3	3
4 L/H	3	3	3	2	2	2	2

APPENDIX C
SOME TABLES AND GRAPHS FOR RELATIVE
PREFERENCE ANALYSIS

TABLE C.1

TOTAL SETUP AND CARRYING COST, SERVICE LEVEL AND BUFFERING COST

EFFECTIVENESS WITH DEGREE OF SUPPLY UNCERTAINTY = 1(H/H)

(Average of Five Runs)

TYPE OF SUPPLY UNCERTAINTY	Buffering Strategy					
	1(SS/SS)	2(SS/SLT)	3(SLT/SLT)	4(SLT/SS)	5(O/O)	6(SS/O)
1(T/T)	5716617. .9015 4.70	8433757. .9014 1.86	11684632. .9412 1.12	10136111. .9411 1.41	4140845. .5850 -	5506390. .8579 4.28
2(Q/Q)	6022291. .9662 4.27	7547021. .9679 2.43	10788702. .9722 1.29	9357132. .9722 1.64	4052835. .7861 -	5215265. .9572 6.89
3(T/Q)	5307630. .9237 4.24	6774632. .9278 2.37	9449184. .9533 1.45	8122208. .9532 1.86	3518008. .7014 -	4537552. .8935 6.58
4(Q/T)	7978082. .9489 3.36	10510178. .9495 1.77	1459282. .9532 .99	12212308. .9532 1.29	5254234. .7536 -	6787520. .9375 5.64

TABLE C.2

TOTAL SETUP AND CARRYING COST, SERVICE LEVEL AND BUFFERING COST

EFFECTIVENESS WITH DEGREE OF SUPPLY UNCERTAINTY = 2(L/L)

(Average of Five Runs)

TYPE OF SUPPLY UNCERTAINTY	Buffering Strategy					
	1(SS/SS)	2(SS/SLT)	3(SLT/SLT)	4(SLT/SS)	5(O/O)	6(SS/O)
1(T/T)	4491037. .9402 8.03	5089676. .9463 4.76	5817591. .9633 4.10	5580978. .9644 4.18	3798475. .8556 -	4275338. .9208 8.94
2(Q/Q)	4909840. .9810 1.25	5422126. .9825 .74	6573204. .9810 .39	6060766. .9810 .49	4156522. .9787 -	4631670. .9809 2.00
3(T/Q)	4529998. .9647 10.64	5052058. .9667 5.79	6004788. .9772 3.82	5480592. .9772 5.22	3880533. .9047 -	4247177. .9586 20.64
4(Q/T)	5625173. .9749 6.11	6384629. .9756 3.48	7690174. .9756 1.95	6919010. .9756 2.61	4687813. .9436 -	5263081. .9718 8.97

TABLE C.3

TOTAL SETUP AND CARRYING COST, SERVICE LEVEL AND BUFFERING COST

EFFECTIVENESS WITH DEGREE OF SUPPLY UNCERTAINTY = 3(H/L)

(Average of Five Runs)

TYPE OF SUPPLY UNCERTAINTY	Buffering Strategy					
	1(SS/SS)	2(SS/SLT)	3(SLT/SLT)	4(SLT/SS)	5(0/0)	6(SS/0)
1(T/T)	5031107. .9254 4.90	5595356. .9335 3.68	8329023. .9541 1.76	5680978. .9404 3.66	3580978. .7389 -	4781046. .9172 5.53
2(Q/Q)	5695553. .9696 5.09	6207214. .9698 3.84	9572210. .9739 1.51	6295208. .9706 3.70	4127314. .8492 -	5421675. .9687 6.12
3(T/Q)	4922469. .9286 5.71	5455774. .9328 4.10	8322444. .9600 1.84	7776051. .9600 2.10	3591623. .7352 -	4675796. .9219 6.89
4(Q/T)	6652067. .9641 4.21	7415191. .9658 3.07	11299634. .9689 1.29	10531587. .9689 1.45	4675067. .8204 -	6296836. .9623 5.04

TABLE C.4

TOTAL SETUP AND CARRYING COST, SERVICE LEVEL AND BUFFERING COST

EFFECTIVENESS WITH DEGREE OF SUPPLY UNCERTAINTY = $4(L/H)$

(Average of Five Runs)

TYPE OF SUPPLY UNCERTAINTY	Buffering Strategy					
	1(SS/SS)	2(SS/SLT)	3(SLT/SLT)	4(SLT/SS)	5(O/O)	6(SS/O)
1(T/T)	7235842. .9178 3.21	10558841. .9365 1.47	11432057. .9531 1.30	9021264. .9519 2.20	5023460. .7867 -	5858185. .8511 5.45
2(Q/Q)	5256403. .9747 3.07	6760785. .9781 1.78	7900914. .9783 1.34	6370693. .9779 2.01	4469439. .9485 -	4836967. .9614 3.23
3(T/Q)	4879885. .9536 7.01	6355802. .9669 3.23	7270832. .9771 2.58	5831007. .9769 4.46	3774232. .8149 -	4077050. .8936 31.71
4(Q/T)	6884038. .9522 4.39	9372527. .9583 2.01	10775550. .9583 1.50	8280555. .9583 2.56	5131293. .8486 -	5699245. .9186 8.99

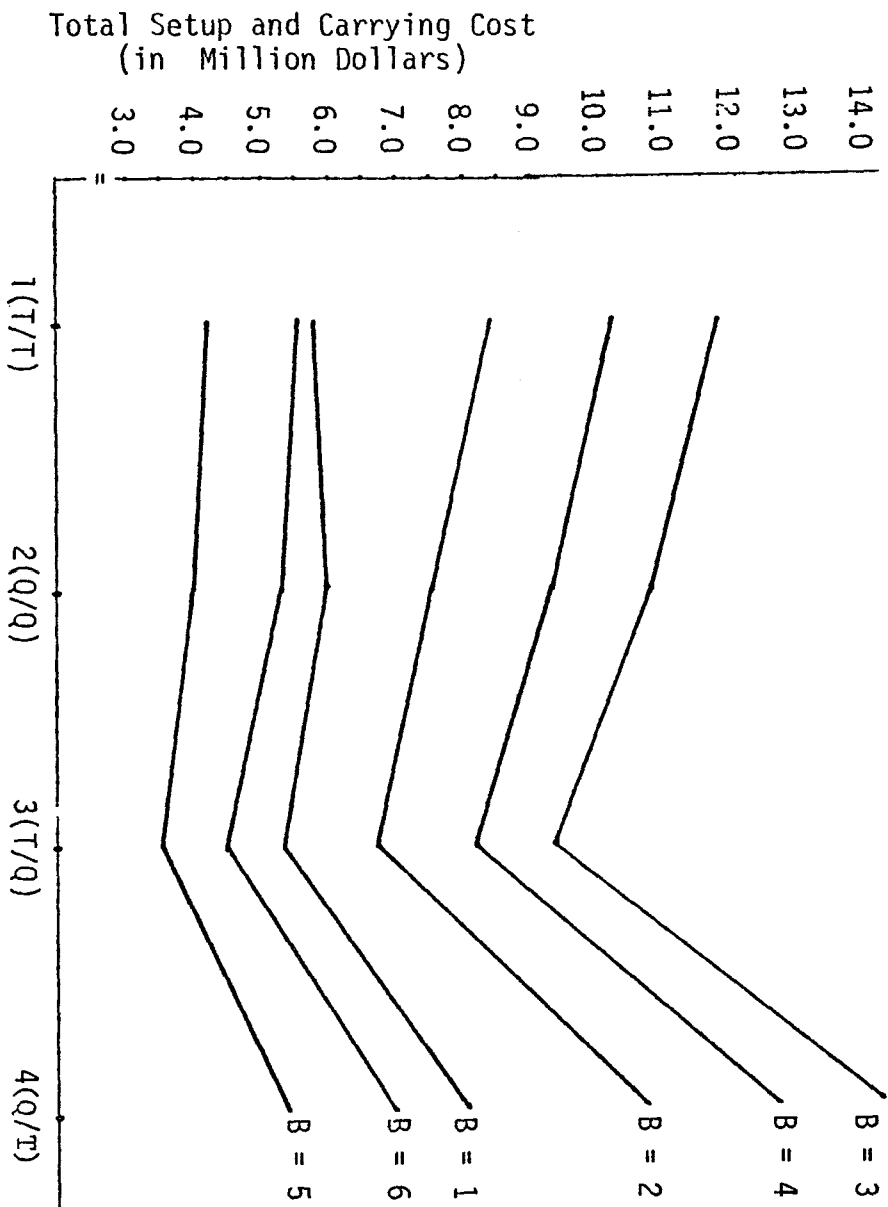


FIGURE C.1 Total Setup and Carrying Cost
Degree of Uncertainty (D) = 1(H/H)

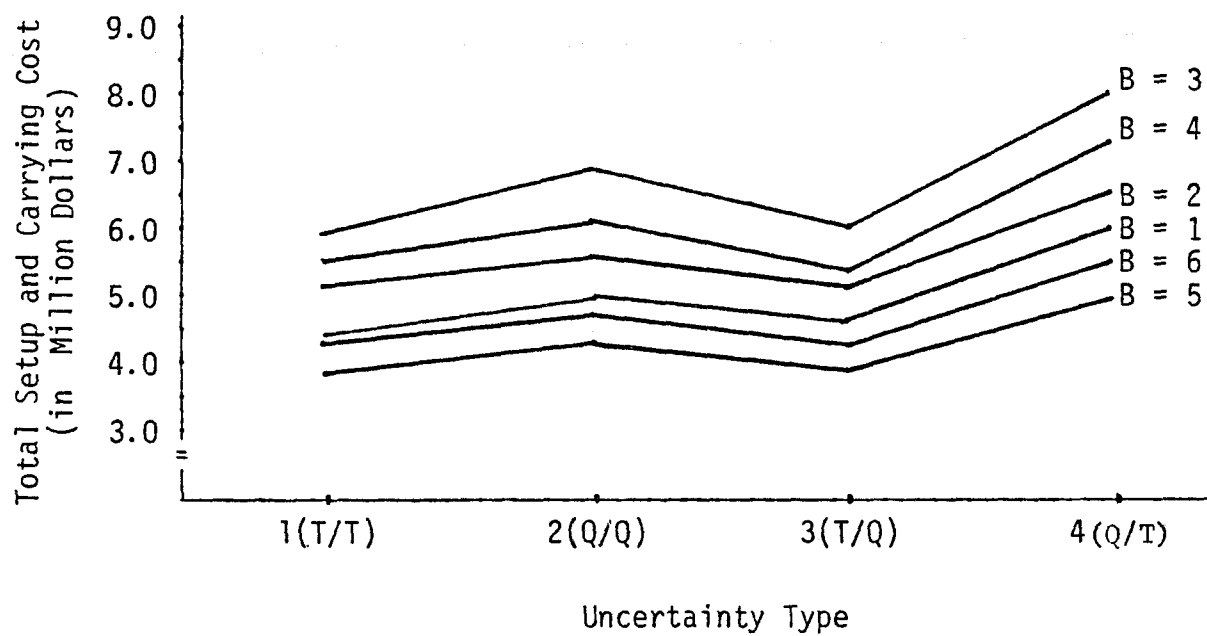


FIGURE C.2 Total Setup and Carrying Cost
Degree of Uncertainty (D)= 2(L/L)

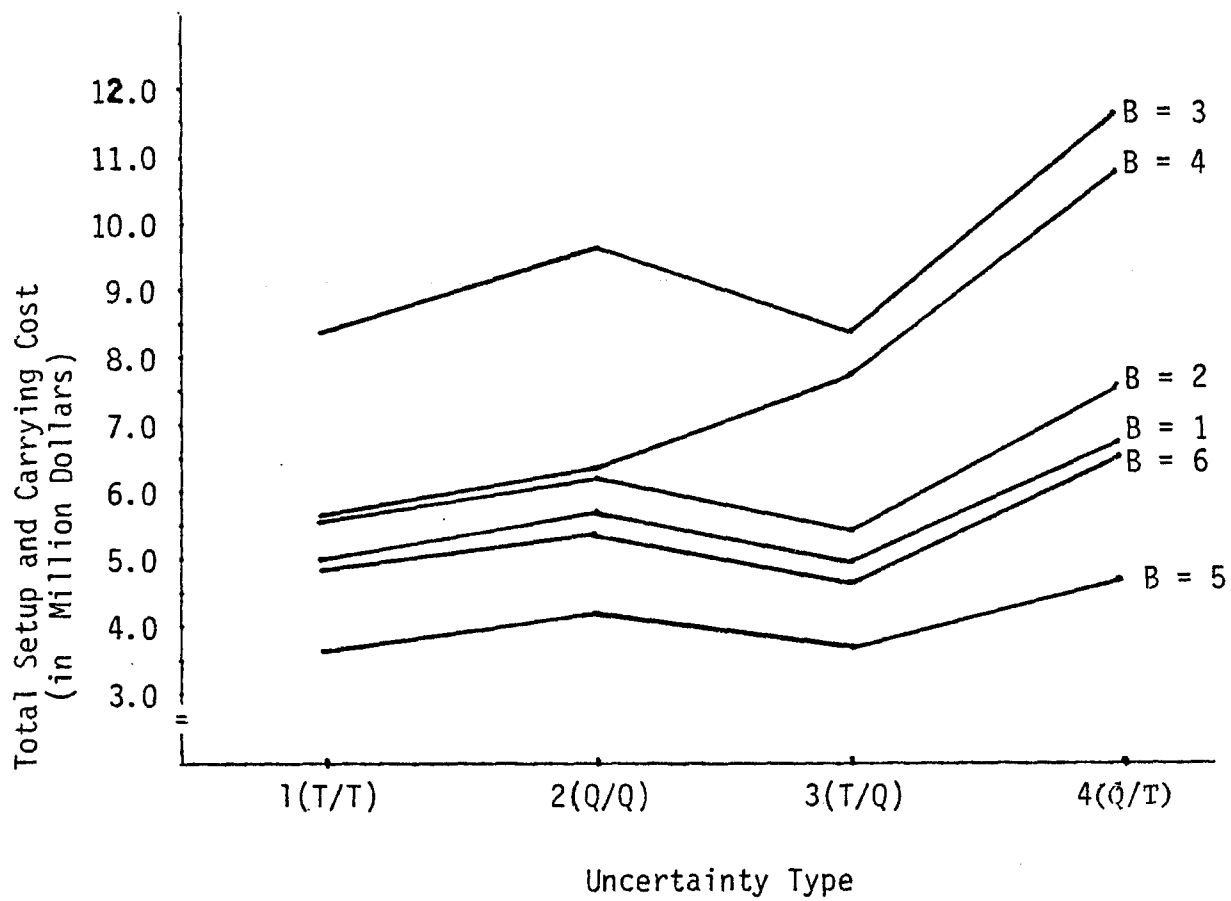


FIGURE C.3 Total Setup and Carrying Cost
Degree of Uncertainty (D)= 3(H/L)

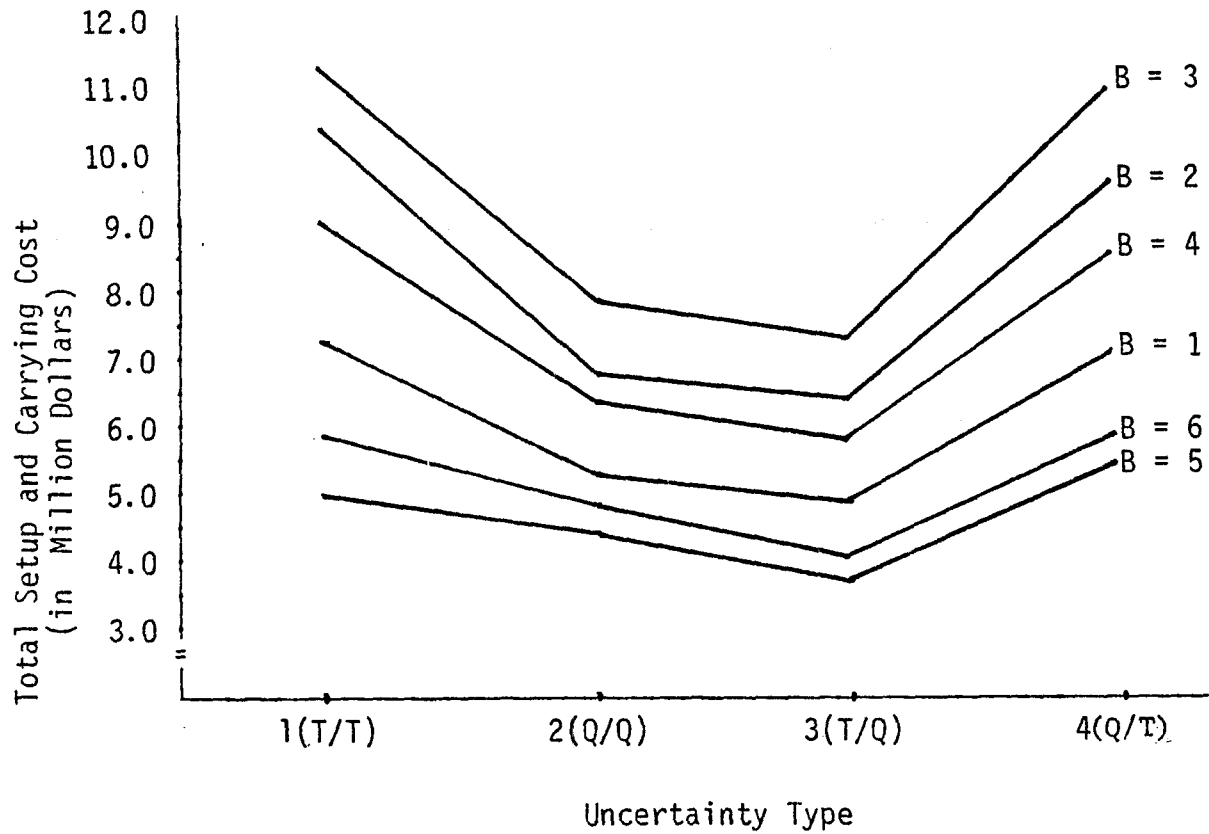


FIGURE C.4 Total Setup and Carrying Cost
Degree of Uncertainty (D) = 4(L/H)

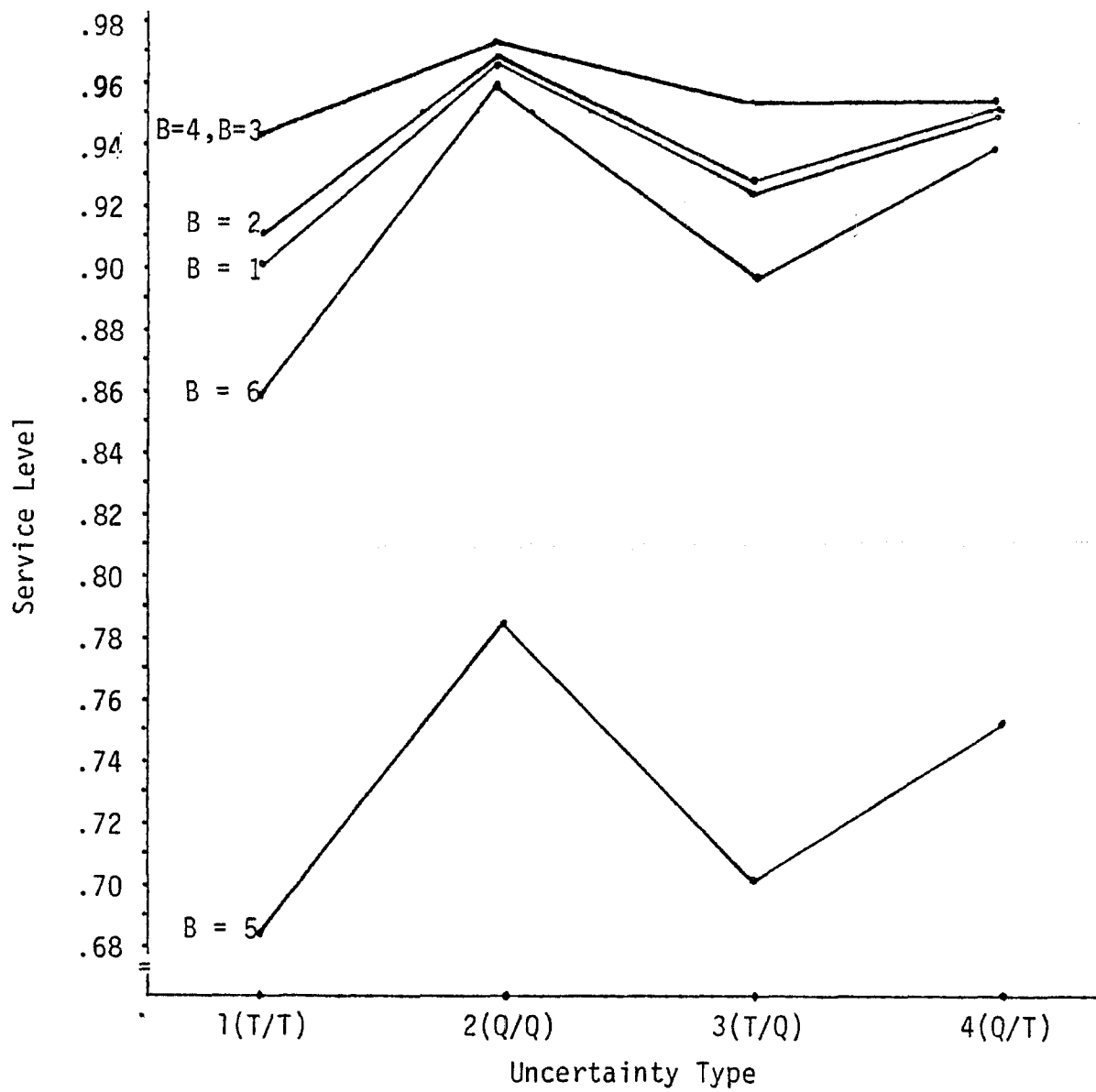


FIGURE C.5 Service Level Values
Degree of Uncertainty (D)= 1(H/H)

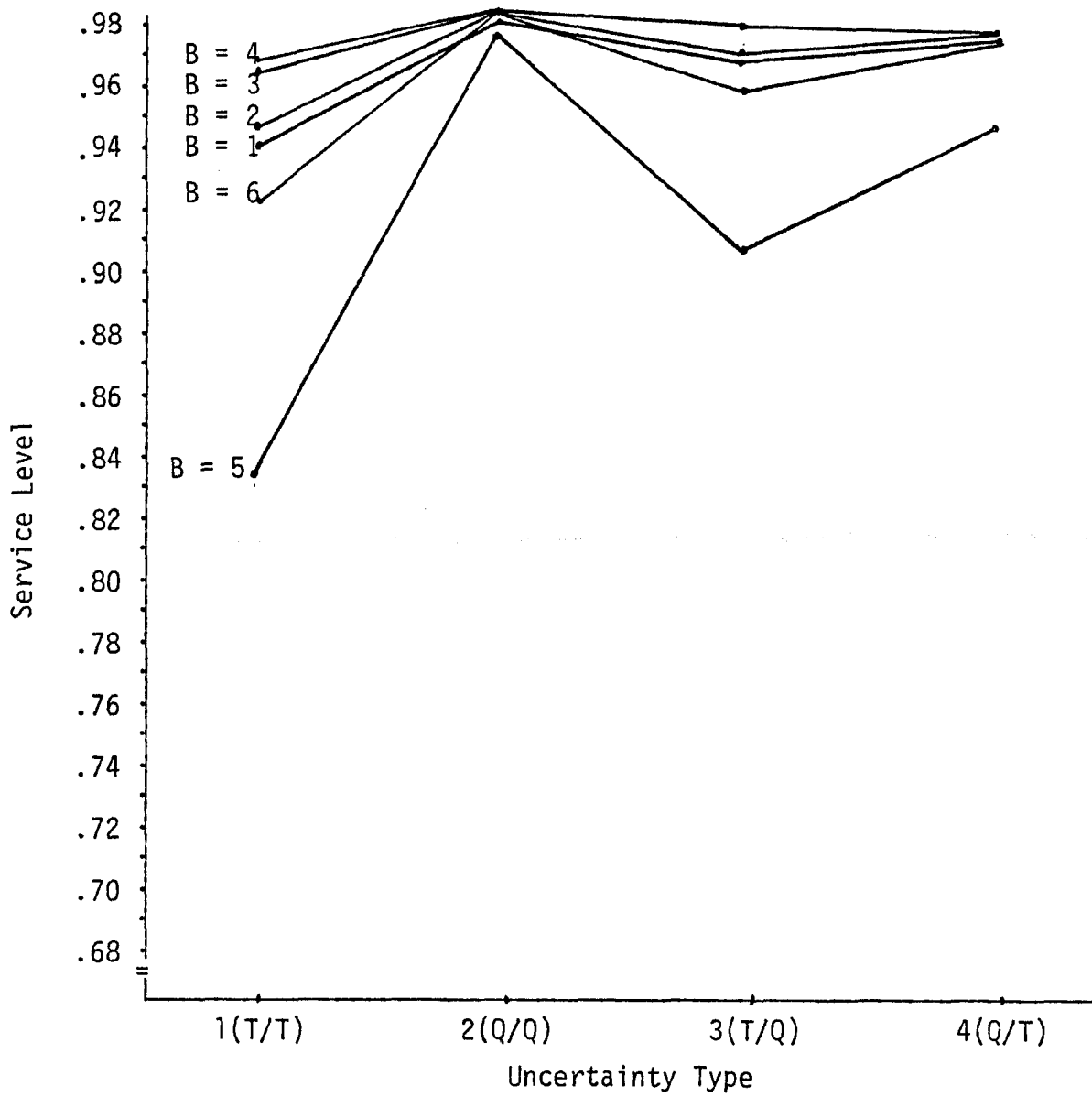


FIGURE C.6 Service Level Values
Degree of Uncertainty (D)= 2(L/L)

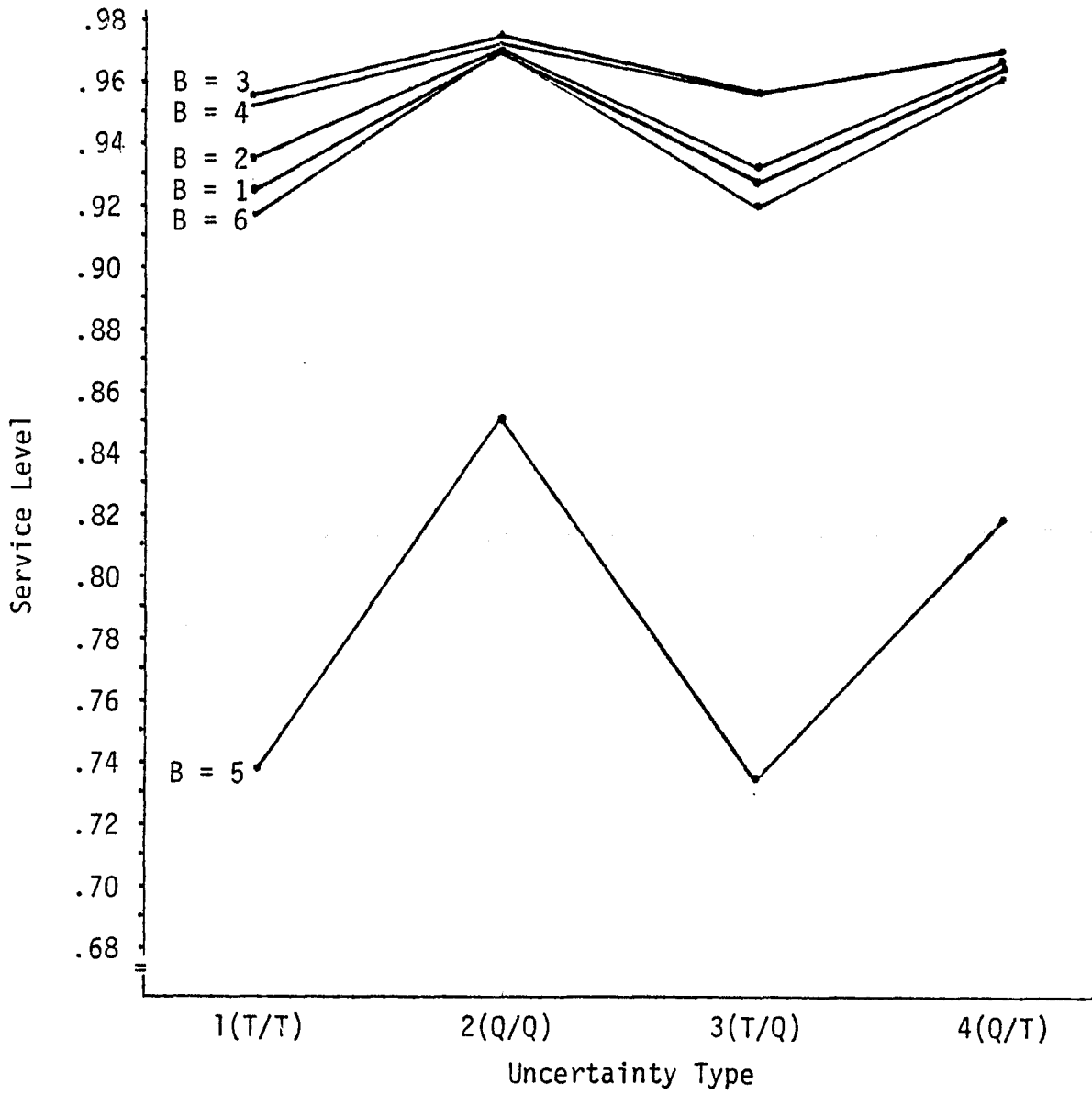


FIGURE C.7 Service Level Values
Degree of Uncertainty (D)= 3(H/L)

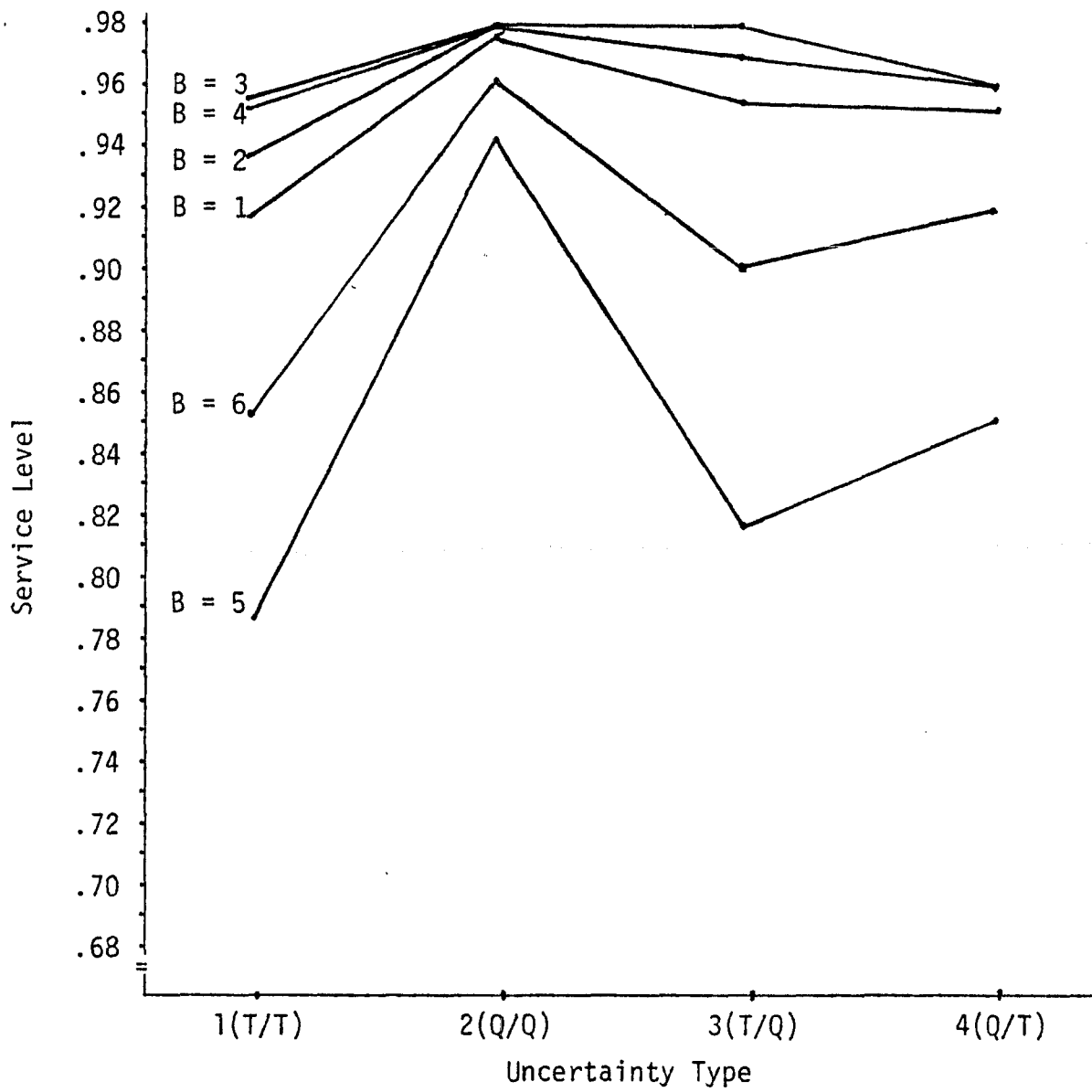


FIGURE C.8 Service Level Values
Degree of Uncertainty (D)= 4(L/H)

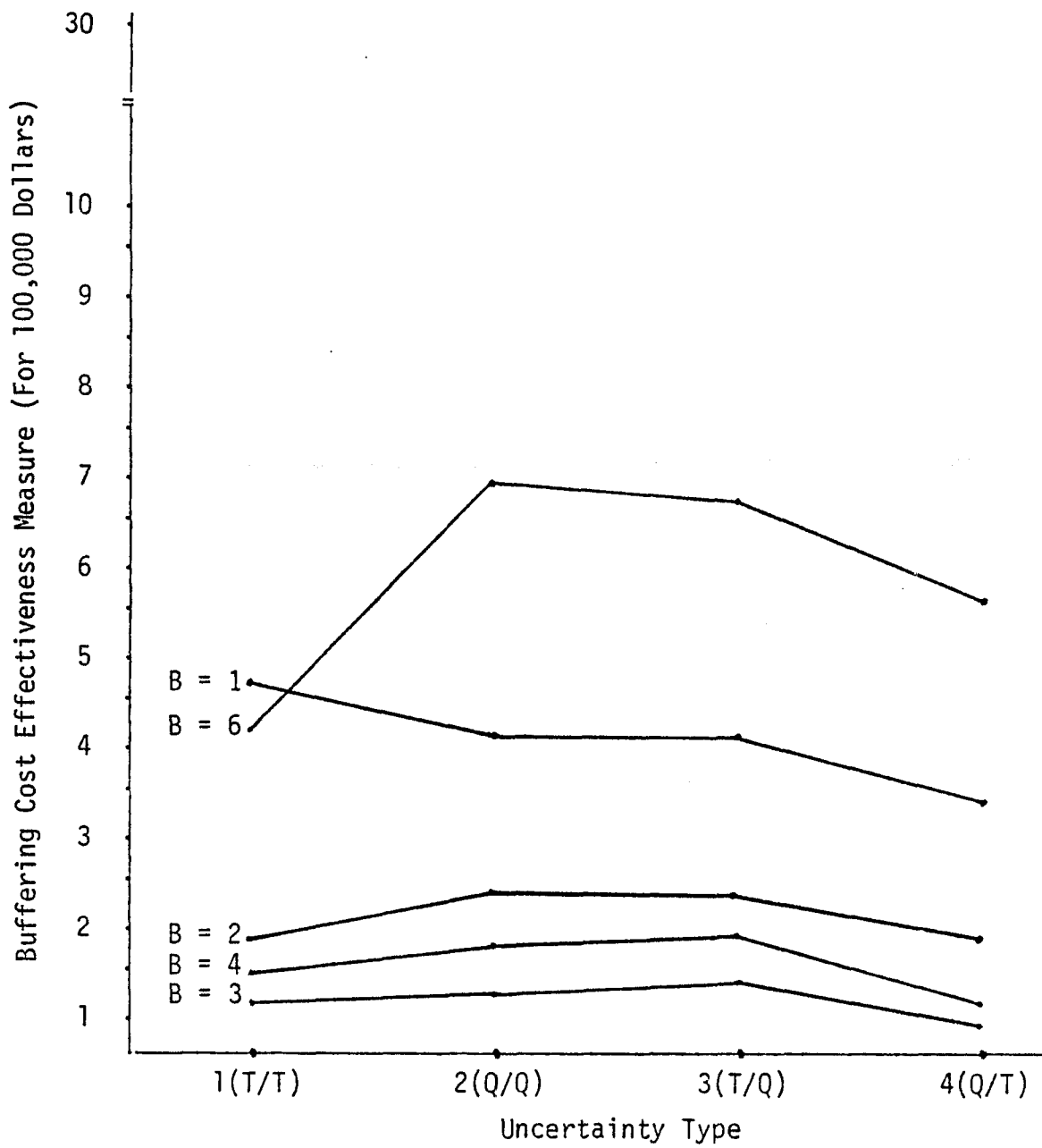


FIGURE C.9 Inventory Rate of Return
Degree of Uncertainty (D) = 1(H/H)

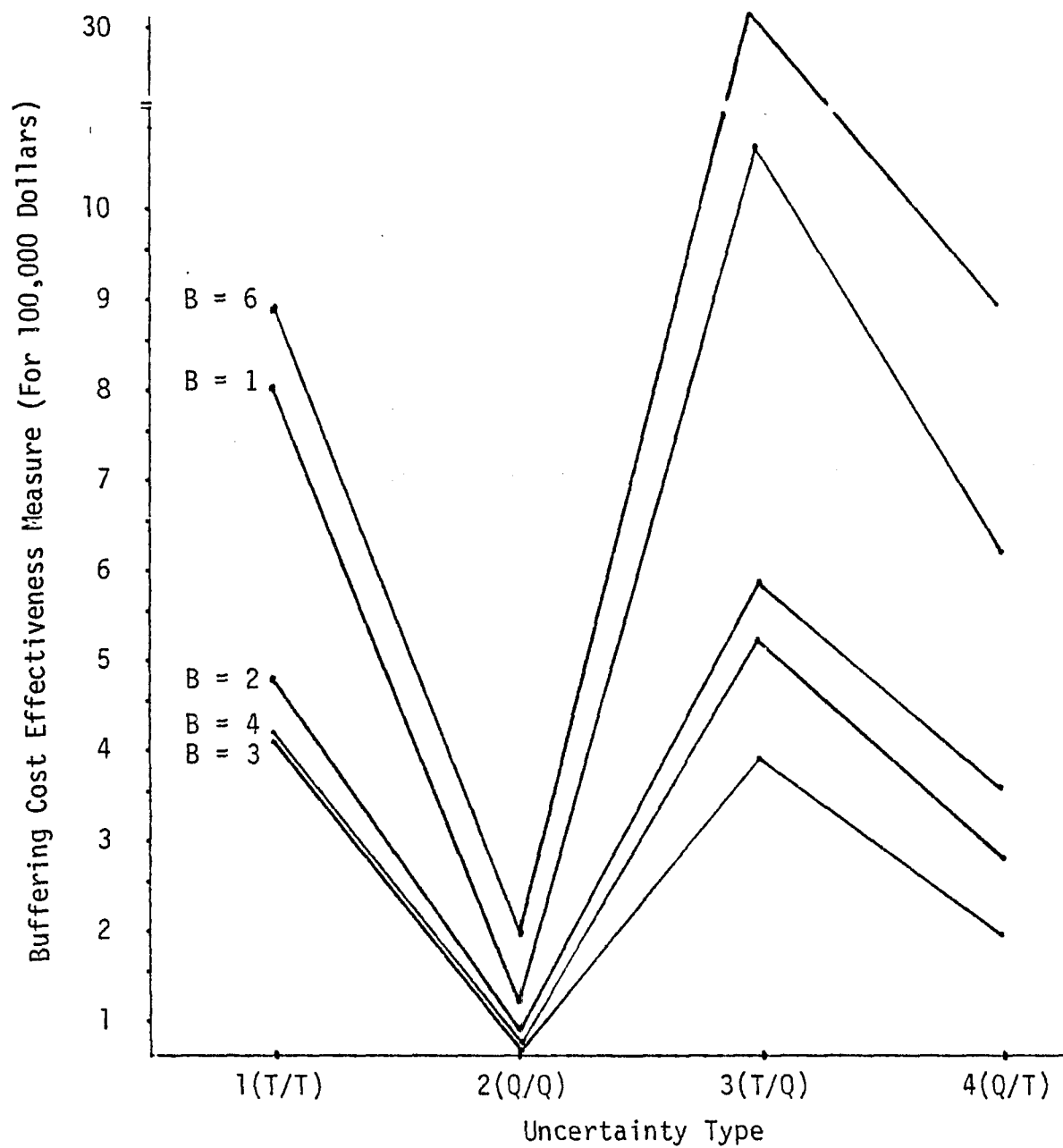


FIGURE C.10 Inventory Rate of Return
Degree of Uncertainty (D) = 2(L/L)

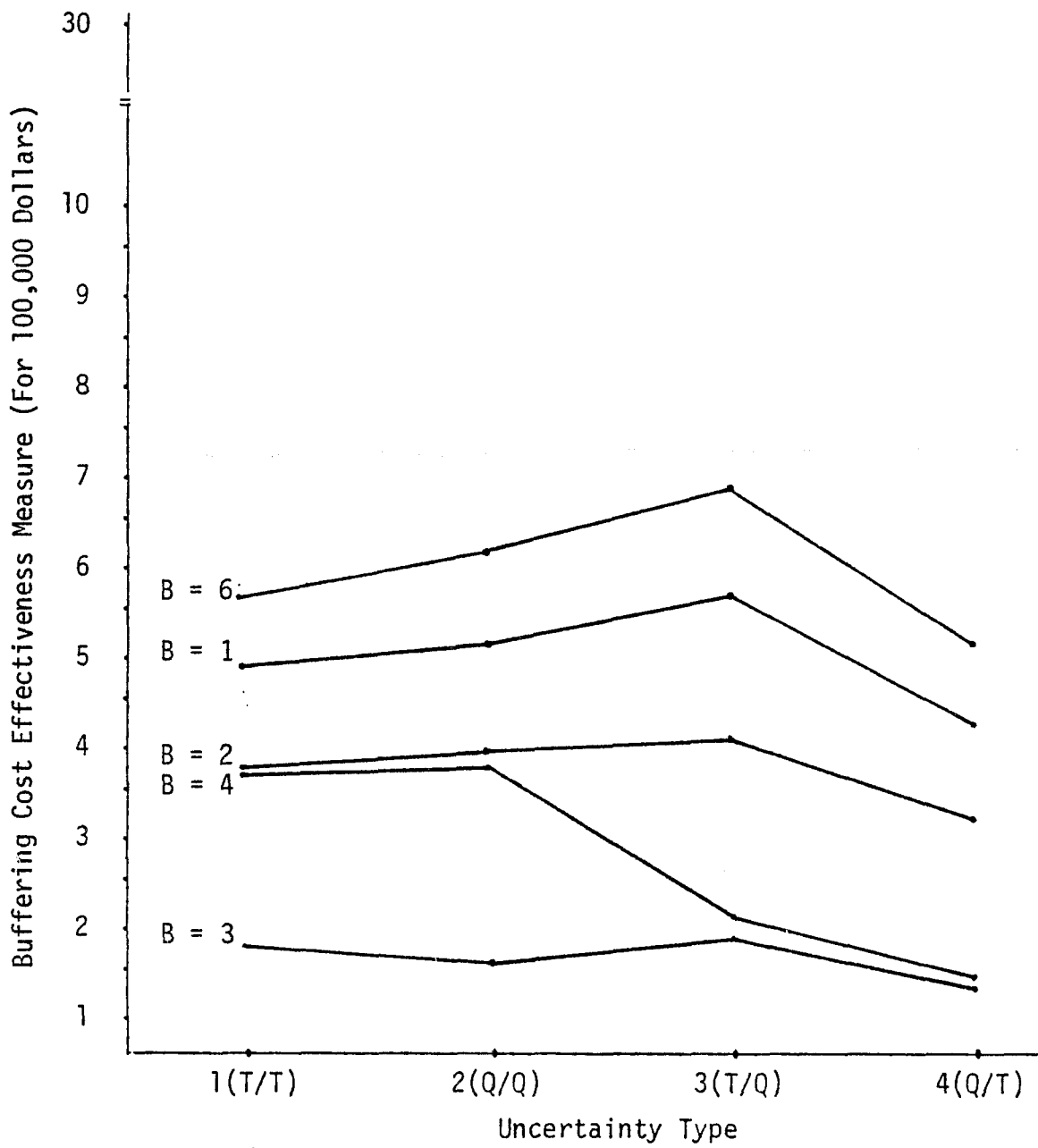


FIGURE C.11 Inventory Rate of Return
Degree of Uncertainty (D) = 3(H/L)

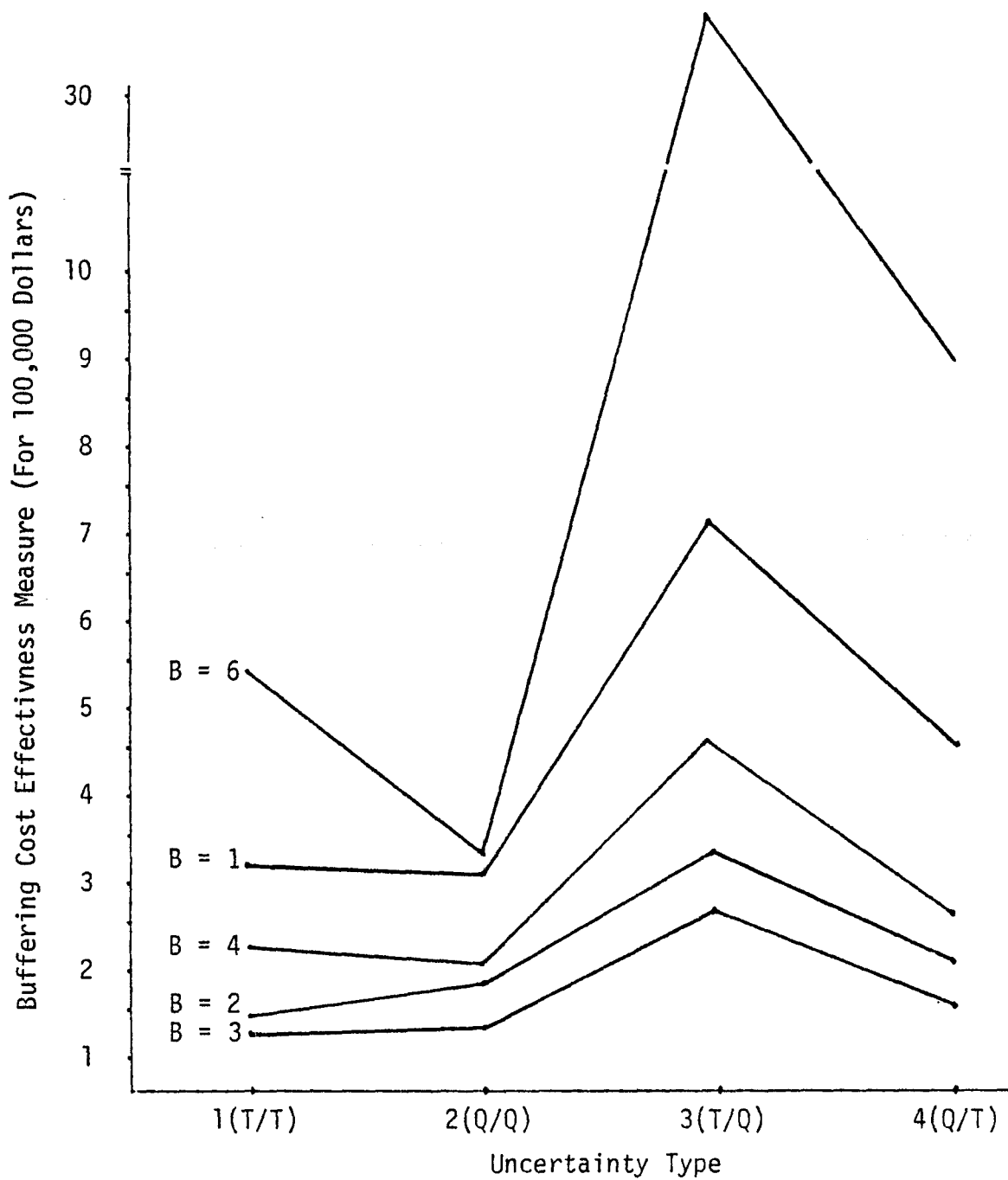


FIGURE C.12 Inventory Rate of Return
Degree of Uncertainty (D) = 4(L/H)

APPENDIX D
SIMULATION PARAMETERS

Three different types of data were required to conduct this study. Some of them are required as an input to the MRP system. The second type is related to the production and replenishment process of all orders released by the MRP stage. The last category is some cost data required to evaluate the performance of the production system as a whole. This appendix presents these three categories of data.

MRP INPUT

The three major inputs of an MRP system are the master production schedule, the product structure records, and the inventory status files. Some details about the information provided in each are reported in this section.

Master Schedule

A deterministic and constant demand by planning period and quantity for end items are stated in the Master Schedule File. Because uncertainty of supply is the only source of risk considered in this study, a deterministic end-item demand was assumed; i.e., a perfect forecast. Also, in order to eliminate the effect of demand variability on the need for safety stocks a constant end-item demand was used. Callarman and Mabert (11) have shown that for very small demand variability, as measured by the coefficient of variation, no safety stock was needed to attain high service levels.

A constant weekly demand of one hundred units, two hundred units, three hundred units and four hundred units, for end items one through four respectively, was provided.

Bill of Materials File

This file includes product structure and the number of units required in each assembly.

There are four end products in the product structure file, each calling for two assembly groups and one raw material. Seven categories of raw materials are used in the assembly process and are assumed to be purchased from outside suppliers. Figure D.1 shows the bill of material with a hierarchy of components in each assembly and subassembly. Parent-component relationship and the number of units of the components required in an assembly or subassembly are also specified in Table D.1. In spite of the fact that degree of commonality is not of major concern in this study, the selected product structure implies the high commonality level case according to Collier's measure for the degree of commonality (15). Commonality degree (C) is equal to 2.33 in this research.

TABLE D.1
Parent-Component Relationship in the
Product Structure File

Parent Item	Component Item	Units Required in Assembly
1	5, 6, 16	One
2	5, 7, 16	One
3	5, 8, 16	One
4	5, 9, 16	One
5	10, 11	One
6	10, 12	One
7	10, 13	One
8	10, 14	One
9	10, 15	One

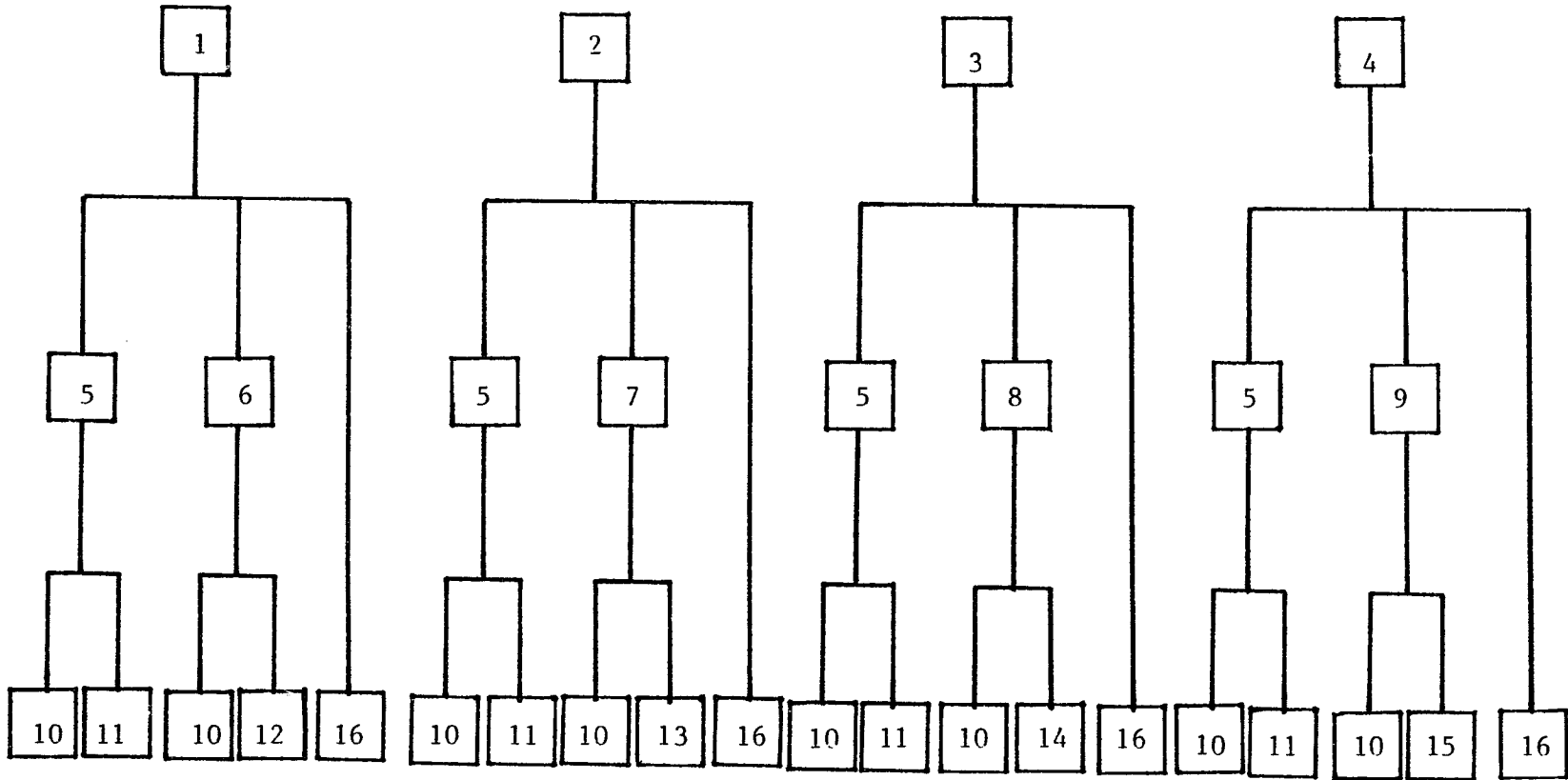


FIGURE D.1 Hierarchy of Bill of Materials

Inventory Files

These files include information about initial inventory, lead time, lot sizing rule, the amount of safety stock and any scheduled receipts for each item in the product structure. The initial inventory for each item was selected at a level that minimizes the warm-up period as indicated in Chapter III. This level is equivalent to one-half period demand for each item. The demand for all intermediate items was derived from the requirements of its parent item(s).

The lead times for all inventory items are assumed to be one period, a week, in the simulation model. For items processed in the factory, this one week includes both setup and processing times.

As for lot sizing rule, a lot-for-lot rule was selected for all items all over the hierarchy. This eliminated the variation in the projected stock due to batching.

The amount of safety stock required for each item was estimated as a function of the degree of supply uncertainty and the desired service level as explained in Chapter III. These values are as follows:

a. D = High (HQ = .3 or HT = 1)

Items	1-8	90	180	270	360	900	90	180	270
Items	9-16	360	1800	900	90	180	270	360	900

b. D = Low (LQ = .1 or LT = .2)

Items	1-8	30	60	90	120	300	30	60	90
Items	9-16	120	600	300	30	60	90	120	300

All scheduled receipts were set to equal zero for all items in this study.

PRODUCTION AND REPLENISHMENT DATA

This set of data includes setup and run times for each item and the amount of capacity available at each department in terms of the size of the work force. Following is a list of both setup and run times in terms of the amount of manhours required.

<u>Item No.</u>	<u>Setup Time</u>							
1 - 8	1000.0	900.0	800.0	700.0	600.0	550.0	500.0	450.0
9 - 16	400.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
<u>Item No.</u>	<u>Run Time</u>							
1 - 8	5.0	3.0	4.0	4.5	3.0	3.0	4.0	2.5
9 - 16	2.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0

The regular capacity available was specified in terms of number of people available in each department as 300, 500 and 5 in departments one, two and three respectively. This is equivalent to 120,000, 20,000 and 200 weekly man-hours (assuming 40 working hours a week). An overtime capacity is also available in each department for situations when the labor requirements exceed the available labor force. It is limited to only 30% of regular time capacity.

COST DATA

The labor cost was set at five dollars per hour in all three departments, while raw material unit costs for items 10 - 16 were as follows:

\$	20.00	5.00	2.00	10.00	50.00	5.00	10.00
----	-------	------	------	-------	-------	------	-------

The unit cost of each item throughout the simulation was calculated based on the cost of its components and the labor cost involved in producing one unit of that item. Carrying cost was set at 24% of the calculated unit cost for each item. A shortage cost per unit of 40% of the unit cost of the item short and an overtime cost set at one and one-half times

the regular time cost were used to calculate the "total cost" performance measure.

APPENDIX E
THE PROGRAM DOCUMENTATION

LIST OF SYMBOLS

- AP(I) = Actual Production of Item I
 BMR(D) = Beginning Item Number for Department D
 BN(D) = Number of Items Made in Department D
 BO(I) = Lost Sales Units for Product I
 C(I) = Per Unit Cost of Item I
 CLOSTS = Lost Sales Cost Per Unit of Stockout
 CM(IP) = Per Unit Cost of Material for Item IP
 COMP(I,L) = The Immediate Lower Level Components for Item I
 COST(1) = Inventory Carrying Cost for the Period
 COST(2) = Setup Cost for the Period
 COST(3) = Total Setup and Carrying Cost for the Period
 COST(4) = Over Time Cost
 COST(5) = Lost Sales Cost
 COST(6) = Idle Time Cost
 COSTPA = Payroll Cost
 COSTY(I) = Year to Date Cost for Cost (I)
 DFG(I,M) = Actual demand for Product I in Period M
 DL = The Amount of Delay (Timing Uncertainty)
 DORDER = Order Processed Or Delivered After the
 Scheduled Date
 FGP(I) = Productivity Factor for Item I
 IINV(I) = Initial Inventory of Product I
 FORCST(I,M) = Forecasted Demand for Product I in Period M
 GROSS(I,M) = Gross Requirements for Item I in Period M
 HSLT = High Safety Lead Time
 IBO = Total Number of Units Short to Date

INV(I,M) = Inventory On Hand Used in the MRP Procedure

JMS(NMS) = Item Number which its Production

KMS(NMS) = Item Which Its Shortage Caused a Reduction in
Production of Item IP

LSLT - Low Safety Lead Time

NMS = A Counter of Number of Material Shortage
Occasions for this Period

LDTIME(I) = Lead Time for Product I

LEVEL(I) = The Lowest Level on the Bill of Material on
which Item I resides

MM = Number of Periods (weeks) being Simulated

NET(I,M) = Net Requirements for Item I in Period M

NFGS = Number of Finished Goods

OB Performance Measure = The Value of this Performance Measure for
One Observation

ORDER(I,M) = Lot Size for Item I in Period M

OTH(D) = Over Time Hours Used in Department D

P = Planning Horizon (12 weeks)

PART = Item Number

PAYCST = Payroll Cost for this Period

PP(N) = A Temporary Storage Variable Used During
MRP Product Explosion

POTH = Over Time Man Hours Used in all Departments
in this Period

PSUH = Setup Man Hours Used in all Departments
in this Period

PXIP = Idle Time Man Hours Incurred in All Departments
in this Period

Q(I) = Number of Immediate Lower Level Components
for Item I

RECPT(I,M) = Schedule Receipt for Item I in Period M

RELS(D,I,M) = Schedule Released for Item I in Period M

RH(D) = Run Man Hours Used in Department D

RUNTIM = Run Time Used to Produce this Item in
this Department

S(I) = Setup Man Hours Incurred if Item I is Produced

SCHED(I,M) = Schedule Receipt for Item I in Period M

SETUP(ID) = Number of Setups in Department ID for
this Period

SETUPS = Total Number of Setups in All Departments
To Date

SFG(I) = Sales of Finished Good I

SSH = High Safety Stock

SSHF = High Safety Stock Factor Used in MRP Calculations

SSL = Low Safety Stock

SSLF = Low Safety Stock Factor Used in MRP Calculations

STH(D) = Straight Time Man Hours Available in Department D

STKOUT = Total Number of Stockouts to Date

SUH(D) = Setup Man Hours Used in Department D

T = The Present Period

TB(I) = Total Number of Units Short of Product I
(Lost Sales)

TBO = Total Units of Lost Sales

TCOST = Period Total Cost

TCOSTY = Year to Date Total Cost

TI = Total Inventory Value this Period

TINVV = Total Inventory Value to Date

TOTLVL = Total Number of Levels in the Bill of Materials

TRH(D) = Total Run Man Hours Used in Department D

TV = Total Inventory Value for this Item in
This Period

TXIH = Total Idle Man Hours in this Period

TYOTH = Total Year to Date Overtime Hours Used in
All Departments

TYSUH = Total Year to Date Setup Hours Used in All
Departments

TYXIH = Total Year to Date Idle Time Hours Used in
All Departments

U(I) = Run Time Per Unit for Item I (MAN HOURS)

US(I) = Units Supplied of Product I Toward its Sale

USAGE(I,J) = Number of Units of the Jth Immediate Lower Level
Component Used to Produce One Unit of Item I

V(I) = Inventory Total \$ Value for Item I

WR = Wage Rate (\$/Man Hours)

X = A Temporary Variable Used to Indicate the Item
Number Being Netted

XI(I) = One Hand Inventory of Item I (Units)

XIC = Inventory Cost (\$/\$ Per Month)

XIH(D) = Idle Man Hours Used in Department D

XLW(D) = Work Force in Department D

XM(J) = Present Period Requirements of Item J

XM1(L,J) = Product Structure Array

XMOT = Maximum Overtime Fraction

XU = Shortage Percentage (Quantity Uncertainty)

Y(PREFIX) = A Variable with a Prefix Y is the Year to Date
Value of the variable that follows Y

Z = A Temporary Variable used to Indicate Per
Unit Value of an Item

The Program Code

Enclosed is one version of the program that has been used in this study. This is the case of HT/HQ uncertainty category with SLT/SS buffering strategy. Number of replications is five in this case.

```

C$JOB          TIME=60,PAGES=55
C
C
1  C          DIMENSION AP(16),BMR(3),BN(3),BO(4),COST(7),COSTY(7),DFG(4,64),
          1FORCST(4,64),JMS(16),JOL(3),KMS(16),SETUP(3),OTH(3),RH(3),
          2S(16),SFG(4),STH(3),SUH(3),TH(4),TRH(3),U(16),US(4),UOC(4),
          3V(16),XIH(3),XLW(3),XM(16),XM1(16,16),YCTH(3),YSETUP(3),NSETUP(3),00040C10
          4CM(16),TOIH(3),TSTH(3),TSUH(3),TTRH(3),COSTAL(7),COSTAV(7),
          5TXIH(3),YRH(3),YSTH(3),YSUH(3),YXIH(3),RATIO(16),XU(16),IRN(5),
          6OTHAL(3),OTHAV(3),XIHAL(3),XIHAV(3),R(6),NSETAL(3),NSETAV(3),
          7DORDER(16,64),OBCO1(5),OBCO3(5),OBCO7(5),OBB0(5),OBBTK(5),
          8OBSLVL(5)
          C
          C00000C1
          C0000C02
          19C10
          2001
          C0080010
          C00090C10
          C0010C10
          C0050C10
          C00070C10
2  C          INTEGER AP,BMR,BN,BO,COMP,DFG,FORCST,GROSS,IINV,INV,JMS,JOL,KMS,KT
          1,LDTIME,LEVEL,MAX,ORDER,P,PP,PART,Q,RECPT,RELSO,SCHED,SETUPS,SFG,
          2T,TH,THO,TOTLVL,US,USAGE,X,XI,XLW,XM,XM1,COLECT,STKOUT,D,DD,SETUP,
          3YSETUP,STKAL,STKAV,VAR1,VAR2,VAR3,VAR4,DORDER,DL,SSL,SSH,SSLF,
          4LSLT,HSLT
          C00090C10
          C0010C10
          C00110C10
          C00120C10
3  C          COMMON/AA/ COMP(9,3),GROSS(16,64),IINV(16),INV(16,64),YFL,DL(16),
          1LEVEL(16),NET(16,64),ORDER(16,64),PART(16),O(9),RECPT(16,64),IX,
          2RELSO(16,64),SCHED(16,64),USAGE(9,3),PP(65),P,MAX,T,X,XI(16),IY,
          3TOTLVL,LDTIME(16),IPP(16),IU(16),KT,LENT(16),MIN(12),D(16),
          4SSL(16),SSH(16),SSLF(16,64),SSH(16,64),HSLT(16),
          5LSLT(16)
          C00130C10
          C00140C10
          C150C10
          C160C10
          C170C10
4  C          COMMON/BB/C(16),CARY(16),SETUPC(16)
          5DOUBLE PRECISION IIX
          6IIX=8931
          C180C10
          C00200C10
          C00210C10
          C00190C10
7  C          IRN(1)=325647745
          8IRN(2)=547746523
          9IRN(3)=455623378
          10IRN(4)=647745523
          11IRN(5)=455247763
          12DO 172 IO=1,3
          13OTHAL(IO)=0.
          14OTHAV(IO)=0.
          15XIHAL(IO)=0.
          16XIHAV(IO)=0.
          17CONTINUE
          172DO 173 K=1,7
          18COSTAL(K)=0.
          19COSTAV(K)=0.
          20CONTINUE
          21173CONTINUE
          22SLAL=0.
          23ASL=0.
          24STKAL=0
          25STKAV=0
          26DO 191 IO=1,5
          27IX=IRN(IO)
          28WRITE(6,799)
          29WRITE(6,801)IO
          30801FORMAT(40X,'***** REPORTS FOR OBSERVATION ',12,' *****
          C**')
          31WRITE(6,799)
          32WRITE(6,799)
          C00890C10
          C0090C10
          C00910C10
          C00920C10
          C00980C10
          C00990C10
          C01010C10
          C01020C10
          C00220C10
          C00230C10
          C00240C10
          C00250C10
C          INITIALIZATION
C          SET CONSTANTS AND CLEAR ARRAYS

```

33	C	VAR1=4	C0260C10
34		VAR2=3	
35		VAR3=1	
36		P=12	00340C10
37		MM=64	
38	C	DO 1 I=1,16	00370C10
39		IF(I.GT.4) GO TO 2	00380C10
40		BO(I)=0	00390C10
41		SFG(I)=0	00400C10
42		TB(I)=0	00410010
43		US(I)=0	00420C10
44		DO 18 M=1,MM	00430C10
45		FORCST(I,M)=0	00440C10
46	18	CONTINUE	00450010
47	C	2 AP(I)=0	00460C10
48		DL(I)=0	00470010
49		XU(I)=0.	00480C10
50		JMS(I)=0	00490C10
51		KMS(I)=0	00500C10
52		V(I)=0.	00510C10
53		XI(I)=0	00520C10
54		XM(I)=0	00530C10
55		DO 19 M=1,MM	00540C10
56		GROSS(I,M)=0	00550C10
57		INV(I,M)=0	00560C10
58		SSHF(I,M)=0	
59		SSLF(I,M)=0	
60		NET(I,M)=0	00570010
61		DDORDER(I,M)=0	
62		ORDER(I,M)=0	00580C10
63		RECPT(I,M)=0	00590C10
64		RELSO(I,M)=0	00600C10
65		SCHED(I,M)=0	00610C10
66	19	CONTINUE	00620C10
67	1	CONTINUE	00630C10
68	C	DO 3 ID=1,3	00640C10
69		JOL(ID)=0	00650C10
70		NSETUP(ID)=0	00660C10
71		NSETUP(ID)=0	00670C10
72		OTH(ID)=0.	00680010
73		RH(ID)=0.	00690010
74		SETUP(ID)=0	00700C10
75		STH(ID)=0.	00710C10
76		SUH(ID)=0.	00720C10
77		TBO=0	00730010
78		TRH(ID)=0.	00740C10
79		TOTH(ID)=0.	00750C10
80		TRH(ID)=0.	00760C10
81		TSIH(ID)=0.	00770010
82		TSUH(ID)=0.	00780C10
83		TTRH(ID)=0.	00790C10
84		TXIH(ID)=0.	00800C10
85		YOTH(ID)=0.	00810010
86		YSETUP(ID)=0	00820C10
87		YRH(ID)=0.	00830C10
88		YSTH(ID)=0.	00840C10
			00850C10

89		YSUH(ID)=0.	00860010
90		YXIH(ID)=0.	00870010
91		XIH(ID)=0.	00880010
92	3	CONTINUE	00930010
	C		00940010
93		DO 5 K=1,7	00950010
94		COST(K)=0.	C0960010
95		COSTY(K)=0.	C0970010
96	5	CONTINUE	01000010
	C		01030010
97		COSTPA=0.	C1040010
98		NMS=00	01050010
99		SETUPS=0	01060010
100		STKOUT=0	01070010
101		TCOST=0.	01080010
102		TCOSTY=0.	01090010
	C	READ IN THE PARAMETER VALUES	01100010
103		READ(5,301)BMR,BN,XLW	01110010
104	301	FORMAT(915)	C1120010
105		READ(5,302)0	01130010
106	302	FORMAT(1612)	01140010
107		MAX=BN(1)+BN(2)+BN(3)	01150010
108		MAT=BN(1)+BN(2)	01160010
109		NFGS=BN(1)	01170010
110		MASY=BMR(2)+1	01180010
111		MATY=BMR(3)+1	01190010
	C		01200010
112		DO 101 I=1,MAT	01210010
113		READ(5,203)(COMP(I,J),J=1,3)	01220010
114	203	FORMAT(315)	01230010
115	101	CONTINUE	01240010
	C		01250010
116		DO 102 I=1,MAT	01260010
117		READ(5,203)(USAGE(I,J),J=1,3)	01270010
118	102	CONTINUE	01280010
	C		01290010
119		DO 103 I=1,MAX	01300010
120		READ(5,304)(XMI(I,J),J=1,MAX)	01310010
121	103	CONTINUE	01320010
	C		01330010
122		DO 104 I=1,NFGS	01340010
123		READ(5,303)(DFG(I,M),M=1,MM)	01350010
124	303	FORMAT(2413)	01360010
125	104	CONTINUE	01370010
126		READ(5,310)CM	01380010
127	310	FORMAT(10X,11F5.0)	01390010
128		READ(5,373)IINV	
129	373	FORMAT(1215)	01410010
130		WRITE(6,695)(I,IINV(I),I=1,MAX)	
131	695	FORMAT(1X,8(2X,(IINV(I),12,''),14))	
132		READ(5,304)LDTIME	01430010
133		READ(5,304)LEVEL	01440010
134	304	FORMAT(1611)	01450010
135		READ(5,302)PART	01460010
136		READ(5,305)S	01470010
137	305	FORMAT(5X,6F10.0)	01480010
138		READ(5,309)U	01490010
139	309	FORMAT(5X,6F10.1)	01500010
140		READ(5,306)V	01510010
141	306	FORMAT(5X,6F10.0)	01520010

142		READ(5,307)P,TOTLVL										01530C10
143	307	FORMAT(5X,2I5)										01540C10
144		READ(5,308)CLOSTS,WR,XIC,XMOT										01550C10
145	308	FORMAT(10X,4F10.2)										015600 0
146		READ(5,719)SSL										
147		READ(5,719)SSH										
148	719	FORMAT(16I4)										
149		PRINT,SSL										
150		PRINT,SSH										
151		READ(5,719)LSLT										
152		READ(5,719)HSLT										
153		PRINT,LSLT										
154		PRINT,HSLT										
155		WRITE(6,799)										01570010
156		WRITE(6,799)										01600C10
157		WRITE(6,799)										
158		WRITE(6,818)										
159	818	FORMAT(2X,'T	COST(1)	COST(3)	TCOST		NMS					
		C BO(1) BO(2) BO(3)	BO(4)	STKOLT	IND		PER					
		CBO')										
160		WRITE(6,799)										
	C											01610010
	C	START OPERATING THE FACTORY										01620C10
	C	OPERATE DEPARTMENTS										01630C10
	C											01640C10
	C											01650010
161		T=0										01660C10
	C											01670C10
162	1000	T=T+1										01680010
163		IPBO=0										
164		NMS=0										01690C10
165	799	FORMAT(' ')										01700C10
	C											01730C10
166		IF(T.EQ.1)GO TO 11										01740C10
167		IF(T.GT.1)GO TO 21										
	C											01760C10
	C											01810C10
	C	START A NEW RUN OF P PERIOD										01820C10
	C											01830C10
	C	CLEAR THE PERFORMANCE MEASURE COLLECTORS										01840C10
	C											01850C10
168	11	DO 12 I=1,7										01860C10
169		COST(I)=0.										01870C10
170		COSTY(I)=0.										01880C10
171	12	CONTINUE										01890C10
172		IBO=0										01900C10
173		DO 13 ID=1,3										01920C10
174		NSETAL(ID)=0										01930C10
175		TOTH(ID)=0.										01940C10
176		YSETUP(ID)=0										01950C10
177		YOTH(ID)=0.										01960010
178		YSTH(ID)=0.										01970010
179		YSUH(ID)=0.										01980010
180		YXIH(ID)=0.										01990C10
181		YRH(ID)=0.										02000C10
182	13	CONTINUE										02010C10
	C											02020C10
183		DO 14 I=1,NFGS										020J0C10
184		BO(I)=0										02040C10
185	14	CONTINUE										02050C10

186		COSTPA=0.	02060C10
187		NMS=0	02070C10
188		SETUPS=0	02080C10
189		STKOUT=0	02090C10
190		TCOSTY=0.	02100C10
191		TITH=0.	02110C10
	C		02120C10
192		TYSUH=0.	02130C10
193		TYOTH=0.	02140C10
194		TYXIH=0.	02150C10
195		TINVV=0.	02160C10
196		IF(T.EQ.1)GO TO 33	02170C10
197		GO TO 21	02180C10
	C		02190C10
198	33	DO 34 I=1,MAX	02200C10
199		JMS(I)=0	02210C10
200		KMS(I)=0	02220C10
201		XI(I) = IINV(I)	02230010
202	34	CONTINUE	02240C10
203	21	KT=T+P-1	
	C		02250C10
	C		02270010
204		DO 1029 I=1,MAX	02280C10
205		DO 1028 M=T,KT	02290C10
206		GROSS(I,M)=0	02300C10
207	1028	CONTINUE	02310C10
208	1029	CONTINUE	02320C10
	C		02330C10
	C	READ DEMAND	
	C		02350010
	C		02360C10
	C		02370010
	C		0238001
209		DO 1039 I=1,NFGS	
210		DO 1038 M=1,KT	
211		GROSS(I,M)=DFG(I,M)	
212	1038	CONTINUE	02440C10
213	1039	CONTINUE	02450010
	C		02460010
	C		02470C10
	C	A- CALCULATION OF YEARLY DEMAND	02490C10
	C		02500C10
214		DO 151 I=1,MAX	02510C10
215		D(I)=0	02520C10
216	151	CONTINUE	02530010
	C		02540C10
217		DO 159 I=1,NFGS	02550C10
218		DO 153 M=1,P	02560C10
219		D(I)=D(I)+GROSS(I,M)	02570010
220	153	CONTINUE	02580010
	C		02590C10
221		DO 157 J=MASY,MAX	02600C10
222		IF(XMI(I,J))157,157,155	02610010
223	155	D(J)=D(J)+D(I)*XMI(I,J)	02620C10
224	157	CONTINUE	02630C10
225	159	CONTINUE	02640C10
	C		02650C10
226		DO 165 I=MASY,MAT	02660C10
227		DO 163 J=MATY,MAX	02670010
228		IF(XMI(I,J))163,163,161	02680C10
229	161	D(J)=D(J)+D(I)*XMI(I,J)	02690C10
230	163	CONTINUE	02700C10

231	165	CONTINUE	02710C10
	C		02720C10
	C	B- CALCULATION OF UNIT COSTS	02730C10
	C		02740010
232		DO 467 I=1,MAX	02750C10
233		IF(T.EQ.1)XI(I)=IINV(I)	02760C10
234		IF(XI(I).EQ.0)GO TO 467	02770010
235		C(I)=V(I)/XI(I)	02780C10
236	467	CONTINUE	02790C10
	C		0280C010
	C		02910C10
	C	CALCULATION OF SETUP AND CARRYING COSTS FOR END ITEMS	02920C10
	C		02930C10
237		DO 171 I=1,MAX	02940C10
238		SETUPC(I)=S(I)*WR	02950010
239		CARY(I)=C(I)*XIC*12	02960C10
240	171	CONTINUE	02970C10
	C		02980C10
	C	CALCULATE SETUP TO INVENTORY CARRYING COST RATIO	02990C10
	C		03000C10
241		DO 7 I=1,MAX	03010C10
242		RATIO(I)=SETUPC(I)/CARY(I)	03020C10
243	7	CONTINUE	03030010
	C		
	C	CALCULATE LOST SALES COST PER UNIT OF END ITEM SHORT	03040C10
	C		
244		DO 8 I=1,NFGS	03050010
245	8	BOC(I)=CLOSTS*C(I)	03060C10
	C		03070010
	C		03250C10
	C		03260C10
	C		03280010
	C		03290C10
246		CALL MRP	03300010
	C		03310C10
	C		03320C10
	C	PRINT ORDERS	03330C10
	C	START DEPARTMENT LOOP	03340010
	C		03350C10
247	35	DO 70 ID=1,3	03360C10
	C		03370C10
	C	ZERO MATERIAL USAGE	03380010
	C		03390C10
248		DO 36 J=1,MAX	03400C10
249	36	XN(J)=0	03410C10
	C	GET MATERIAL LOWER AND UPPER LIMITS FOR THIS DEPARTMENT	03420010
250		IL=BMR(ID)+I	03430C10
251		IU=BMR(ID)+BN(ID)	03440010
	C	COMPUTE MATERIAL REQUIREMENTS	03450C10
	C		03460010
252		DO 38 IP=IL,IU	03470010
253		IF(IP.GT.MAT)GO TO 854	
254		DL(IP)=0	
255		KLF=0	
256		TOTAL=0	
257	920	CALL RANDU(IX,IY,YFL)	
258		G=1.-YFL	
259		WX=-1.*ALOG(G)	
260		TOTAL=TOTAL+WX	
261		IF(TOTAL.GE.1)GO TO 975	

262		KLF=KLF+1	
263		GO TO 920	
264	975	UL(IP)=KLF	
265		IF(DL(IP).LT.1)GO TO 853	
266		K=T*DL(IP)	
267		DORDER(IP,K)=ORDER(IP,T)+DORDER(IP,K)	
268		ORDER(IP,T)=DORDER(IP,T)	
269		GO TO 854	
270	853	ORDER(IP,T)=ORDER(IP,T)+DORDER(IP,T)	
271	854	DO 37 IZ=1,MAX	
272		XM(IZ)=XM(IZ)+XMI(IP,IZ)*ORDER(IP,T)	
273	37	CONTINUE	
274	38	CONTINUE	03500010
	C		03510C10
275		DO 49 J=1,MAX	03520C10
	C	CHECK MATERIAL AVAILABILITY	03530C10
	C		
276		IF(XI(J))39,40,40	03540C10
277	39	XI(J)=0	03550010
278		V(J)=0	03560C10
279	40	CONTINUE	03570010
280		IF(XM(J)-XI(J))49,49,41	03580010
	C	THERE IS A SHORTAGE OF ITEM J	03590010
281	41	AB=XI(J)	03600C10
282		AC=XM(J)	03610C10
283		F=AB/AC	03620C10
	C	REDUCE DESIRED PRODUCTION	03630C10
	C		03640C10
284		DO 48 IP=IL,IU	03650010
285		IF (XMI(IP,J)-1)48,42,42	03660010
286	42	CONTINUE	03670010
287	43	{F(ORDER(IP,T))46,46,44	03680C10
288	44	CONTINUE	03690C10
	C	ADD = OF MATERIAL SHORTAGE OCCASIONS FOR THIS PERIOD	03700010
289		NMS=NMS+1	03710C10
	C	ITEM WHICH ITS PRODUCTION WAS CUT BECAUSE OF SHORTAGE OF ITEM J	03720C10
	C	JMS(NMS)=IP	03730C10
	C	ITEM WHICH ITS SHORTAGE CAUSED A REDUCTION IN PRODUCTION OF ITEM J	03740010
	C	KMS(NMS)=J	03750010
290	46	ITEMP=ORDER(IP,T)	03760C10
	C	ADJUSTED PRODUCTION PLANS 0	03770010
291		ORDER(IP,T)=F*ORDER(IP,T)	03780C10
292		IR=ORDER(IP,T)-ITEMP	03790C10
	C		03800C10
293		DO 47 IZ=MASY,MAX	03810C10
294	47	XM(IZ)=XM(IZ)+XMI(IP,IZ)*IR	03820C10
295	48	CONTINUE	03830C10
296	49	CONTINUE	03840C10
	C	END AVAILABILITY CHECK	03850C10
	C		03860C10
	C	ZERO MAN HOUR REQS	03870C10
	C	TR=TOTAL RUN TIME REQUIRED IN THE DEPT FOR THE PERIOD	03880C10
	C	TS=TOTAL SETUP TIME REQUIRED IN THE DEPT FOR THE PERIOD	03890C10
	C	TT=TOTAL SETUP AND RUN TIME REQUIRED IN THE DEPT FOR THE PERIOD	03900C10
297		TT=0.	03910C10
298		TS=0	03920C10
299		TR=0.	03930C10
	C	GET MAN HOUR REQS	03940C10
	C		03950010
300		DO 51 IP=IL,IU	03960010

301		IF(ORDER(IP,T))51,51,50	03970010
302	50	TS=TS+S(IP)	03980010
303		TR=TR+ORDER(IP,T)*U(IP)	03990010
304		NSETUP(ID)=NSETUP(ID)+1	04000010
305	51	CONTINUE	04010010
306		TT=TR+TS	04020010
	C		
	C	NOW WE HAVE MAN HOUR REQS IN DEPT(ID)	04030010
	C	STRAIGHT TIME MAN HOURS IN DEPT(ID)	04040010
307		ST=40.*XLW(ID)	
	C		
	C	CHECK OVERTIME AND CALC OVER AND IDLE TIME	04060010
308		IF(TT-ST) 52,52,53	04070010
	C		
	C	AMPLE STRAIGHT MAN-HOURS AVAILABLE IN DEPT(ID)	04080010
309	52	OTH(ID)=0.	04090010
310		XIH(ID)=ST-TT	04100010
311		F=1	04110010
312		GO TO 64	04120010
	C	AVAILABLE STRAIGHT MAN-HOURS IN DEPT(ID) IS NOT SUFFICIENT	04130010
313	53	F=TT/ST	04140010
314		WRITE(6,26)ID,T,F	04150010
315	26	FORMAT(10X,'F (OTH FACTOR) FOR DEPT',12,'FOR PERIOD',13,' IS ',	04160010
		*F10.2)	04170010
316	54	CONTINUE	04180010
317		IF(F-XMOT) 56,56,57	04190010
318	56	F=1.	04200010
319		GO TO 63	04210010
	C		
	C	GET FACTOR TO REDUCE PRODUCTION	
320	57	F=XMOT/F	04230010
321		WRITE(6,27)ID,T,F	04240010
322	27	FORMAT(10X,'FF(OTH FACTOR) FOR DEPT',12,' FOR PERIOD',13,' IS ',	04250010
		*F10.2)	04260010
	C	NOL=NOL+1	04270010
	C	JOL(NOL)=ID	04280010
323		TT=XMOT*ST	04290010
324		IF(TT-TS)61,61,62	04300010
325	61	F=0	04310010
326		TT=ST	04320010
327		GO TO 63	04330010
328	62	F=(TT-TS)/TR	04340010
329		WRITE(6,28)ID,T,F	04350010
330	28	FORMAT(10X,'FFF(OTH FACTOR)FOR DEPT',12,' FOR PERIOD',13,' IS ',	04360010
		*F10.2)	04370010
331	63	OTH(ID)=TT-ST	04380010
332		XIH(ID)=0.	04390010
333	64	TR=0.	04400010
334		TS=0.	04410010
	C		
	C	OVERTIME COST FUDGE FACTOR	04420010
335		G=((ST+1.5*OTH(ID))/(ST+OTH(ID)))*WR	04430010
	C		
	C	REDUCE PRODUCTION IF NECESSARY AND ADD SETUP AND RUN TIME	04440010
336		SETUP(ID)=0	04450010
337	164	DO 69 IP=IL,IU	04460010
338		ORDER(IP,T)=F*ORDER(IP,T)	04470010
	C		
339		IF(IP.LE.MAT)GO TO 947	
340		CALL RANDU(IX,IY,YFL)	

341		W=1-YFL	
342		XU(IP)=-.3*ALOG(W)	
343		SP=XU(IP)	
344		ORDER(IP,T)=(1-SP)*ORDER(IP,T)	
	C		
	C		
	C		
	C	ACTUAL = OF UNITS PRODUCED 0	04480010
345	947	AP(IP)=ORDER(IP,T)	
346		IF(ORDER(IP,T)) 69,69,65	04560C10
347	65	TS=TS+S(IP)	04510010
348		SETUP(ID)=SETUP(ID)+1	04520C10
349		RUNTIM=ORDER(IP,T)+U(IP)	04570C10
350		TR=TR+RUNTIM	04540010
	C		
	C	ADD IN LABOR COST FOR THIS ITEM (IN THIS DEPT)	04550C10
351		TL=(S(IP)+RUNTIM)*G	04560010
352		TV=TL	04570010
353		IF(IP.LE.MAT)GO TO 265	04580C10
354		TV=TL+ORDER(IP,T)*CM(IP)	04590C10
355		GO TO 68	04600C10
	C		
356	265	DO 67 IZ=MASY,MAX	04610C10
357		IF (XMI(IP,IZ)-1)67,66,66	04620C10
358	66	IF (XI(IZ)) 465,465,166	04630C10
359	465	Z=0.	04640C10
360		V(IZ)=0.	04650C10
361		GO TO 167	04660C10
362	166	Z=V(IZ)/XI(IZ)	04670C10
	C	VALUE ADDED FROM INVENTORY	04680C10
363	167	TV=TV+ORDER(IP,T)*XMI(IP,IZ)	04690C10
364		XI(IZ)=XI(IZ)-ORDER(IP,T)*XMI(IP,IZ)	04700010
365		V(IZ)=XI(IZ)*Z	
366	67	CONTINUE	04710010
	C		04720C10
	C	ADD OUTPUT INVENTORY UNITS AND VALUE	04730C10
	C	UPDATE THE END OF THE PERIOD INVENTORY VALUE FOR ITEM IP	04740C10
367	68	XI(IP)=XI(IP)+ORDER(IP,T)	04750C10
368		V(IP)=V(IP)+TV	04770010
369	69	CONTINUE	04780C10
	C		
	C	END OF PRODUCTION	04790C10
	C		
	C	RECORD STRAIGHT TIME HOURS	0480C010
	C	STRAIGHT TIME MAN-HOURS AVAILABLE IN DEPT(ID)	04810C10
370		STH(ID)=ST	04820C10
	C		
	C	SETUP MAN-HOURS USED IN DEPT(ID)	04830C10
371		SUH(ID)=TS	04840C10
	C		
	C	RUN MAN-HOURS USED IN DEPT(ID)	04850C10
372		RH(ID)=TR	04860C10
	C		04870010
	C	PAYROLL COST FOR THIS PERIOD 0	04880010
373		PAYCST=(ST +1.5*OTH(ID))*WR	04890C10
	C	TOTAL CGST OF PAYROLL IN ALL DEPTS TO DATE	0490C010
374		COSTPA= COSTPA + PAYCST	04910010
	C		04920010
	C	COLLECT DATA FOR TOTAL PERIODS	04930C10
375		YOTH(ID)=YOTH(ID)+OTH(ID)	04940010

376		YRH(ID)=YRH(ID)+TR	04950C10
377		YSTH(ID)=YSTH(ID)+ST	04960010
378		YSUH(ID)=YSUH(ID)+TS	04970C10
379		YXIH(ID)=YXIH(ID)+XIH(ID)	04980C10
380	70	CONTINUE	04990C10
	C		05000C10
	C		05010C10
	C	END OF DEPARTMENT LOOP	05020C10
	C		05030C10
381		POTH=0.	05040C10
382		PSUH=0.	05050C10
383		PXIH=0.	05060C10
	C		05070010
	C		05080C10
384		DO 71 ID=1,3	05090C10
385		POTH=POTH+OTH(ID)	05100C10
386		PSUH=PSUH+SUH(ID)	05110C10
387		PXIH=PXIH+XIH(ID)	05120C10
388		YSETUP(ID)=YSETUP(ID)+SETUP(ID)	05130C10
389		SETUPS =SETUPS+YSETUP(ID)	05140010
390		TYSUH=TYSUH+YSUH(ID)	05150C10
391		TYOTH=TYOTH+YOTH(ID)	05160C10
392		TYXIH=TYXIH+YXIH(ID)	05170C10
393	71	CONTINUE	05180010
	C		05190C10
	C	START DEMAND AND SALES CALCULATION	05200C10
	C	FINISHED GOODS PRODUCT ITERATION	05210C10
	C		05220C10
394		COST(5)=0.	05230010
395		DO 75 I=1,NFGS	05240C10
	C	CHECK IF ENOUGH INVENTORY	05250C10
396		IF(XI(I)-DFG(I,T)) 72,73,73	05260C10
	C	SHORTAGE OF FINISHED GOOD I	05270010
397	72	US(I)=XI(I)	05280C10
	C	COUNT NUMBER OF UNITS SHORT	05290C10
398		BO(I)=DFG(I,T)-XI(I)	05300C10
399		IPBO=IPBO+BO(I)	05310C10
400		IBO=IBO+BO(I)	05320C10
	C	ADD NUMBER OF STOCKOUTS T	05330C10
401		STKOUT=STKOUT+I	05340C10
402		XI(I)=0	05350C10
403		V(I)=0.	05360C10
404		GO TO 74	05370010
	C	THERE IS SUFFICIENT AMOUNT OF INVENTORY OF FINISHED GOOD I	05380C10
405	73	US(I)=DFG(I,T)	05390C10
406		RO(I)=0	05400C10
407	174	Z=V(I)/XI(I)	05410C10
	C	REDUCE UNITS AND VALUE FOR AMOUNT SUPPLIED	05420010
408	175	V(I)=V(I)-US(I)*Z	05430C10
409		XI(I)=XI(I)-US(I)	05440010
	C	LOST SALES COST (SHORTAGE COST)	05450C10
410	74	COST(5)=COST(5)+BOC(I)*RO(I)	05460C10
411	75	CONTINUE	05470C10
	C		05480010
	C	END OF FINISHED GOODS LOOP	05490010
	C		05500C10
	C	INVENTORY TOTALS FOR YEAR AND INV HOLDING COST	05510010
412		TI=0.	05520C10
413		DO 80 IP=1,MAX	05530010


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456      OBSTK(10)=STKOUT
457      OBSLVL(10)=SRLVL
458      191 CONTINUE
459      DO 187 I=1,7
460      COSTAV(I)=COSTAL(I)/5.
461      187 CONTINUE
C
462      DO 188 ID=1,3
463      NSETAV(ID)=NSETAL(ID)/5
464      OTHAV(ID)=OTHAL(ID)/5.
465      XIHAV(ID)=XIHAL(ID)/5.
466      188 CONTINUE
467      STKAV=STKAL/5.
468      ASL=SLAL/5.
469      WRITE(6,799)
470      WRITE(6,200)
471      200 FORMAT(35X,'***** END OF THE SIMULATION REPORTS OF THE AVERAGES
(
****')
472      WRITE(6,799)
473      WRITE(6,506)
474      506 FORMAT(3X,'OBS      B T D      HOLD.COST      TINV.COST      TOT.
,COST      TOT.BAKOR      STKOUT      SERV.LEVEL')
475      DO 505 IO=1,5
476      WRITE(6,507)IO,VAR1,VAR2,VAR3,CBCO1(IO),CBCO3(IO),OBCO7(IO),OBCO(I
),O),OBSTK(IO),OBSLVL(IO)
477      WRITE(7,508)IO,VAR1,VAR2,VAR3,OUCO1(IO),OBCO3(IO),OBCO7(IO),OPUC(I
),O),OBSTK(IO),OBSLVL(IO)
478      507 FORMAT(4X,12.5X,11.2X,11.2X,11.5X,F9.0,5X,F9.0,5X,F9.0,5X,F8.0,
5X,F4.0,5X,F9.6)
479      508 FORMAT(1X,12.2X,11.2X,11.2X,11.2X,F9.0,2X,F9.0,2X,F9.0,2X,F8.0,2X,
CF4.0,2X,F9.6)
480      505 CONTINUE
481      WRITE(6,799)
482      WRITE(6,96)(I,COSTAV(I),I=1,7)
483      96 FORMAT(7(' CAV(' ,I1,' )=' ,F9.0))
484      WRITE(6,799)
485      WRITE(6,97)(ID,OTHAV(ID),ID=1,3)
486      97 FORMAT(3(' OTHAV(' ,I1,' )=' ,F8.0))
487      WRITE(6,799)
488      WRITE(6,98)(ID,XIHAV(ID),ID=1,3)
489      98 FORMAT(3(' XIHAV(' ,I1,' )=' ,F8.0))
490      WRITE(6,799)
491      WRITE(6,99)STKAV
492      99 FORMAT(1X,'STKAV=' ,I6)
493      WRITE(6,799)
494      WRITE(6,504)ASL
495      504 FORMAT(1X,'AV.SERVICE LEVEL = ' ,F8.6)
496      WRITE(6,100)(ID,NSETAV(ID),ID=1,3)
497      100 FORMAT(3(' NSETAV(' ,I1,' )=' ,I6))
498      WRITE(6,799)
499      190 STOP
500      END
C
C
C
C
C
C
C
C
501      SURROUTINE MRP
C
C      MRP PROGRAM

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06750C10
06770010
06780C10
06790C10
06830C10
06880C10
069C0C10
06910C10
06920C10
06930C10
06940C10
06950C10
06960C10
06975010
06980C10
06990C10
07000C10
07010C10
07020C10
07030C10
07040C10
07050C10
0706C01
07070010
07080C10
07100010
07110C10
07120C10
07130C10
07670C10
07680C10
07690C10

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502	C	INTEGER AP,BMR,BN,BO,COMP,DFG,FORCST,GROSS,IINV,INV,JMS,JCL,KMS,KT 1,LOTIME,LEVEL,MAX,ORDER,P,PP,PART,Q,RECPT,RELSD,SCHED,SETUPS,SFG, 2T,TB,TBO,TOTVL,US,USAGE,X,XI,XLW,XM,XM1,COLECT,STKOUT,C,CC,SETUP, 3YSETUP,STKAL,STKAV,VAR1,VAR2,VAR3,VAR4,ORDER,DL,SSL,SSH,SSLF, 4LSLT,HSLT	07700C10 07710C10 07720C10 07730C10 00120C10
503	C	COMMON/AA/ COMP(9,3),GROSS(16,64),IINV(16),INV(16,64),YFL,DL(16), 1LEVEL(16),NET(16,64),ORDER(16,64),PART(16),Q(9),RECPT(16,64),IX, 2RELSD(16,64),SCHED(16,64),USAGE(9,3),PP(65),P,MAX,T,X,XI(16),IY, 3TOTLVL,LOTIME(16),IPP(16),IQ(16),KT,LENT(16),MIN(12),D(16), 4SSL(16),SSH(16),SSLF(16,64),SSHF(16,64),HSLT(16), 5LSLT(16)	07740C10 00140C10 150010 160C10 170C10
504	C	COMMON/BB/C(16),CARY(16),SETUPC(16)	160C10
	C	MAIN ROUTINE	07800C10
	C	1. FIND ALL COMPONETS ON THIS CURRENT LEVEL	07810C10 07820C10 07830C10 07840C10 07850C10
505	C	KT=T+P-1	07860C10
506	C	DO 30 I=1,MAX	07870C10
507	C	DO 29 M=T,KT	07880C10
508	C	RELSD(I,M)=0	07890C10
509	C	29 CONTINUE	07900C10
510	C	30 CONTINUE	07910C10
511	C	40 DO 50 I= 1,3	07920C10
512	C	K = I - 1	07930010
513	C	IM = 0	07940C10
514	C	DO 43 J = 1,MAX	07950C10
515	C	IF (LEVEL (J) .NE. K) GO TO 43	07960C10
516	C	IM=IM+1	07970010
517	C	PP(IM) = PART (J)	07980010
518	C	43 CONTINUE	07990C10
519	C	N = I	08000C10
520	C	45 X = PP(N)	08010C10 08020010 08030C10
	C	2. CALL NETTING PROCESS	08040C10 08050C10
521	C	INV (X,1) = IINV (X)	08060C10
522	C	CALL NETOUT	08070C10 08080C10
	C	3. DETERMINE IF ALL COMPONENTS ON THIS LEVEL HAVE BEEN NETTED OF THEIR IMMEDIATE COMPONENTS UPDATED IN THEIR GROSS REQUIREMENTS WRITE OUT NETTING-HORIZON	08090C10 08100C10 08110C10
523	C	N=N+1	08120C10
524	C	IF (N.LE.IM) GO TO 45	08130C10
525	C	50 CONTINUE	08140C10
526	C	190 RETURN	08150C10
527	C	END	08160C10
528	C	SUBROUTINE NETOUT	07140C10 07150C10 07160C10
529	C	INTEGER AP,BMR,BN,BO,COMP,DFG,FORCST,GROSS,IINV,INV,JMS,JCL,KMS,KT 1,LOTIME,LEVEL,MAX,ORDER,P,PP,PART,Q,RECPT,RELSD,SCHED,SERUPS,SFG, 2T,TB,TBO,TOTVL,US,USAGE,X,XI,XLW,XM,XM1,COLECT,STKOUT,C,DD,SETUP, 3YSETUP,STKAL,STKAV,VAR1,VAR2,VAR3,VAR4,DORDER,DL,SSL,SSH,SSLF, 4LSLT,HSLT	07170010 07180C10 07730C10 00120C10

530	C	COMMON/AA/ COMP(9,3),GROSS(16,64),IINV(16),INV(16,64),YFL,DL(16),	07200C10
		1LEVEL(16),NET(16,64),ORDER(16,64),PART(16),O(9),RECPT(16,64),IX,	00140C10
		2RELS(16,64),SCHED(16,64),USAGE(9,3),FP(65),P,MAX,T,X,XI(16),IY,	150C10
		3TOTLVL,LDTIME(16),IPP(16),IQ(16),KT,LENT(16),MIN(12),D(16),	160C10
		4SSL(16),SSH(16),SSLF(16,64),SSHf(16,64),HSLT(16),	170010
		SLSLT(16)	
531	C	COMMON/BB/C(16),CARY(16),SETUPC(16)	180010
			07260C10
532		MAT=9	
533		SSLF(X,T)=SSL(X)	
534		SSHf(X,T)=SSH(X)	
535		INV(X,T)=XI(X)	07270C10
536		JT=T+P-1	07280C10
537		DO 40 M=T,JT	07290C10
538		IF(X.LE.9)GO TO 777	
539		NET(X,M)=GROSS(X,M)+SSHf(X,M)-SCHED(X,M)-INV(X,M)	
540		GO TO 888	
541	777	NET(X,M)=GROSS(X,M)-SCHED(X,M)-INV(X,M)	
542	888	M1=M+1	
543		IF(NET(X,M).GE.0)GO TO 5	07320C10
544		IF(NET(X,M).LT.0)GO TO 10	07330C10
545	5	INV(X,M1)=0	07340C10
546		GO TO 15	07350C10
547	10	INV(X,M1)=IABS(NET(X,M))	07360C10
548		NET(X,M)=0	07370C10
549	15	RECPT(X,M)=NET(X,M)	
550		IF(X.GT.MAT)GO TO 999	
551		DD=M-LDTIME(X)-HSLT(X)	
552		GO TO 666	
553	999	DD=M-LDTIME(X)	
554	666	IF(DD.LE.T)GO TO 20	
555		RELS(X,DD)=RECPT(X,M)	07410C10
556		GO TO 40	07420C10
557	20	RELS(X,T)=RELS(X,T)+RECPT(X,M)	07430C10
558	40	CONTINUE	07440010
			07450C10
			07460010
			07470010
559	C	CALL LOT SIZE SUBROUTINE	07480010
560	C	IF (LEVEL(X).EQ.0)CALL LFL	07490C10
		IF (LEVEL(X).NE.0)CALL LFL	07500C10
			07510010
			07520C10
561	C	ENTER GROSS REQUIREMENTS INTO APPROPRIATE MONTHS OF IMMEDIATE	
		LOWER LEVEL COMPONENTS	07530C10
562		MAT=9	07540C10
563		IF(X.GT.MAT)GO TO 55	07550C10
564		IH=1	07560C10
565	48	Z = COMP (X, IH)	07570C10
566		IF (Z.EQ.0)GO TO 55	
567		DO 52 M=T,JT	
568		GROSS(Z,M)=GROSS(Z,M)+ORDER(X,M)+USAGE(X,IH)	07610C10
569	52	CONTINUE	07620C10
570		IF(IH.EQ.3)GO TO 55	
571		IH = IH+1	07630010
572		GO TO 48	07640C10
573	55	RETURN	07650C10
		END	07660C10
574	C	SUBROUTINE LFL	09890C10
			09900C10


```

C
575 INTEGER AP,BMR,BN,BO,COMP,DFG,FORCST,GROSS,IINV,INV,JMS,JCL,KMS,KT 09910C10
1,LDTIME,LEVEL,MAX,ORDER,P,PP,PART,Q,RECPT,RELSD,SCHED,SETUPS,SFG, 09920C10
2T,TR,TBO,TOTVL,US,USAGE,X,XI,XLW,XM,XMI,COLECT,STKOUT,D,DD,SETUP, 09930C10
3YSETUP,STKAL,STKAV,VARI,VAR2,VAR3,VAR4,DORDER,DL,SSL,SSH,SSLF, 07730010
4LSLT,HSLT 00120C10

C
576 COMMON/AA/ COMP(9,3),GROSS(16,64),IINV(16),INV(16,64),YFL,DL(16), 09950010
1LEVEL(16),NET(16,64),ORDER(16,64),PART(16),Q(9),RECPT(16,64),IX, 00140C10
2RELSD(16,64),SCHED(16,64),USAGE(9,3),PP(65),P,MAX,I,X,XI(16),IY, 150C10
3TOTLVL,LDTIME(16),IPP(16),IQ(16),KT,LENT(16),MIN(12),D(16), 160C10
4SSL(16),SSH(16),SSLF(16,64),SSH(16,64),HSLT(16), 170010
5LSLT(16)

577 COMMON/BR/C(16),CARY(16),SETUPC(16) 180C10

C
579 DO 10 M=T,KT 10010C10
579 ORDER(X,M)=RELSD(X,M) 10020C10
580 10 CONTINUE 10030C10

C
581 RETURN 10040C10
582 END 10050C10
10060C10
10070C10

583 SUBROUTINE RANDU(IX,IY,YFL)
584 IY=IX*65339
585 IF(IY) 5,6,6
586 5 IY=IY+2147483647+1
587 6 YFL=IY
588 YFL=YFL*.4656613E-9
589 IX=IY
590 RETURN
591 END

```

C\$ENTRY

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VITA

M. Tawfik Mady was born on April 10, 1947 in Berket El-Saba, Egypt. His elementary and high school education was completed in the Berket El-Saba, Egypt public schools in 1963. He majored in Business Administration at Cairo University, receiving his B.S. with the Second Honors degree in 1967 and an M.B.A. degree in 1974. During his graduate studies at Cairo University, he taught courses in the Department of Business Administration. After receiving his M.B.A., he went to the Sudan for two years on a special teaching assignment at Cairo University in Khartoum. His academic life in the U.S.A. started in Raleigh, North Carolina in the fall of 1976. In June 1978, he received his M.S. in Management with a GPA of 3.67. In August of 1978 he entered the Graduate School of Louisiana State University to work toward the degree of Doctor of Philosophy in the school of Business Administration. During the course of his studies, he majored in production/operations management and minored in quantitative methods. From September of 1980 to December of 1982, he served as a teaching assistant, teaching production/operations management in the Department of Management and the Department of Quantitative Business Analysis. He is a member of The Academy of Management, APICS, AIDS, and TIMS/ORSA.

Mr. Mady is married to former Claire Dessouky. They have three children, Tarek, Zeyad and Sarah.


EXAMINATION AND THESIS REPORT

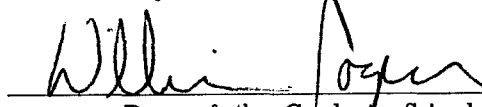
Candidate: Mohamed T. Aly Mady

Major Field: Business Administration (Management)

Title of Thesis: The Effect of Alternative Buffering Techniques to
Protect a Multi-Product, Multi-Stage Production
Inventory System Against Supply Uncertainty

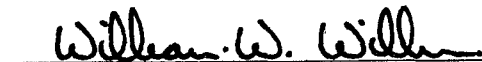
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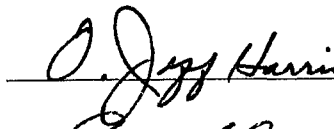

Major Professor and Chairman


Dean of the Graduate School

EXAMINING COMMITTEE:









Date of Examination:

July 15, 1983